

Deep Borehole Instrumentation along San Francisco Bay Bridges - 2001

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May 1, 2001

U.S. Department of Energy

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This work was performed under the auspices of the U. S. Department of Energy by the University of California, Lawrence Livermore National Laboratory under Contract No. W-7405-Eng-48.

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Deep Borehole Instrumentation along San Francisco Bay Bridges - 2001

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March 1, 2001

Abstract

This is a progress report on the Bay Bridges downhole network. Between 2 and 8 instruments have been spaced along the Dumbarton, San Mateo, Bay, and San Rafael bridges in San Francisco Bay, California. The instruments will provide multiple use data that is important to geotechnical, structural engineering, and seismological studies. The holes are between 100 and 1000 ft deep and were drilled by Caltrans. There are twenty-one sensor packages at fifteen sites. The downhole instrument package contains a three component HS-1 seismometer and three orthogonal Wilcox 731 accelerometers, and is capable of recording a micro g from local $M=1.0$ earthquakes to 0.5 g strong ground motion from large Bay Area earthquakes. This report lists earthquakes and stations where recordings were obtained during the period February 29, 2000 to November 11, 2000. Also, preliminary results on noise analysis for up and down hole recordings at Yerba Buena Island is presented.

This work was performed under the auspices of the U.S. Department of Energy by University of California Lawrence Livermore National Laboratory under contract No. W-7405-Eng-48.

Introduction

This is a progress report on the Bay Bridges downhole network. The Bay Bridges down hole network consists of recordings in bore holes that are drilled 100 ft into bedrock along and in the San Francisco Bay (Figure 1). Between 1 and 8 instruments have been spaced along the Dumbarton, San Mateo, Bay, Carquinez, and San Rafael bridges. Tables 1 - 5 list recording site information, and Figure 1 shows instrument locations. In addition, two vertical arrays exist at the Dumbarton bridge with additional sensors at the surface and at 200 ft (Table 1). Two sensors are currently located at the surface at the Bay Bridge and are waiting drill holes. Prior to this study few seismic recording instruments existed in bedrock in San Francisco Bay. This left a recording gap for engineering studies of the Bay bridges and in seismicity studies of the Bay Area. The Bridges network is part of a larger Hayward Fault Digital Network, see Figure 1.

There are six primary areas of research by LLNL that will be enhanced by the bore hole instrumentation: 1) developing realistic predictions of strong ground motion at multiple input points along long span bridges, 2) examining ground motion variability in bedrock, 3) calibrating soil response models, 4) developing bridge response calculations with multiple support input motions, 5) evaluate the seismicity of potentially active faults in the San Francisco Bay, and 6) record strong ground motion.

Key to these studies is LLNL's effort to exploit the information available in weak ground motions (generally from earthquakes $< M=3.0$) to enhance predictions of seismic hazards. Although strong ground motion recordings are essential to calibrate models and understand the hazard of future earthquakes, we can obtain weak ground motion data immediately, whereas it may be years before strong motion data is recorded. Following is an expansion of research goals utilizing recordings from the Bridges Network.

- 1) *prediction of strong ground motion*: LLNL is developing a methodology of using weak ground motion to synthesize linear response strong ground motion and incorporating this with constraints on fault rupture scenarios to predict strong ground motion. These computations provide estimates of the full wavetrain ground motion at multiple points along long span structures.
- 2) *ground motion variability*: Recent studies have demonstrated the high variability of strong ground motion with site conditions. Recordings along Bay bridges will be used both to improve calculations of ground motions for bridges, and to research the spatial sensitivity and significance of site variability to structures.
- 3) *soils response*: LLNL is researching means of using weak ground motion to constrain soils models for non-linear computations. Current research has shown that low strain constitutive properties are significant to non-linear ground motion computations, and that these values can be significantly improved by an iterative process of matching weak motion solutions.
- 4) *bridge response calculations*: Current developments in structural dynamics allow non-linear, three-dimensional calculation of bridge response. This requires realistic full wavetrain input ground motions. LLNL is conducting research on the sensitivity of synthetic ground motions

to accurate non-linear computations, and the significance of utilizing multiple support input calculations.

- 5) *seismicity*: Location of small earthquakes within the Bay that may indicate the existence of active faults will be made possible with the instrumentation. Very small earthquakes ($M < 2$) cannot be recorded adequately to determine accurate locations by regional networks.
- 6) *strong ground motion*: Strong ground motion from previous earthquakes gives a good indication of what might be expected from future earthquakes. In addition recent earthquakes have demonstrated the high variability of strong ground motion so that an array of strong ground motion recordings will give a better understanding of the ground motion variability from future earthquakes.

Instrumentation

As a result of collaboration between the Berkeley Seismographic Station Hayward Fault Network, Lawrence Livermore National Laboratory, and Caltrans, a seismic network of eight instruments was installed in boreholes (one surface recorder awaits a borehole) along the SFOBB (Hutchings et al, 1999). In addition, a temporary surface recorder was installed above the borehole on the east side of YBI near Pier E2 of the SFOBB. Tables 1-5 list the recording site locations for instruments at all bridges in this study. Table 6 lists instrument orientations, previously discussed in report for 1999. Figure 1 shows the location of the bridges.

The down-hole sensor package is manufactured at LBL under the direction to Dr. Tom McEvilly, and is the same package used by the USGS and LBL for the Hayward Fault Digital Recording Network. This package contains three orthogonal Oyo HS-1 4.5 Hz geophones and a three orthogonal Wilcoxon 731s 10v/g accelerometers. The dynamic range of the Wilcoxon package is from a micro-g to 0.5 g acceleration, and is flat to frequency response from 0.1 to 300 Hz. This allows recording of $M = 1.0$ to 0.5 g strong ground motion from large Bay Area earthquakes. Typically, the Wilcoxon's are recorded over two dynamic ranges to capture weak and strong ground motions, and HS-1's are used as a backup for weak ground motion recording. Portable Refraction Technology 72A Data Acquisition Systems with 16 bit resolution and 200 Hz sampling are used to record the data at most sites. Three sites utilize Quantera-4120 24-bit resolution data loggers with 500 Hz recorders. The data is processed and managed at UC Berkeley. Tables 1-5 list site and instrumentation information for the recording sites.

Table 7 lists the events located at the Bay Bridge during this period. Table 8 lists the events recorded at each station.

Preliminary Results

A temporary surface recorder was installed above the borehole on the east side of YBI. Figure 2 shows the location of the borehole on YBI (located at 37.8143 N, -122.3582 W). The uphole site is referred to as BE2U and the downhole site is referred to as BE2D. We identified 18 events that were recorded on both the top and bottom of the borehole (Table 9). Locations and magnitudes listed in Table 9 are from the Northern California Earthquake Data Center (UCB, 1999). The locations of the 18 events are plotted in Figure 2.

BE2U has a reftek recorder and a S-6000 seismometer, and BE2D has a Quanterra recorder and Wilcoxon 731s 10v/g accelerometers. BE2D also contains three orthogonal Oyo HS-1, 4.5 Hz geophones for backup. The dynamic range of the Wilcoxon package is from a micro-g to 0.5 g acceleration, and typically records nearby microearthquakes greater than about $M=1.0$ as well as strong ground motion. The S-6000 clips at accelerations near 0.002 g, so we are limited to recordings smaller or distant events at BE2U.

We have removed the response of each system to get ground motion to the frequency limit of the systems. The Wilcoxon accelerometers and Quanterra recorder (downhole system) are flat for acceleration from 0.1 Hz to the anti-alias filter at 100 Hz. The low frequency limit is from a high pass filter in the power box. It is down 3 db at 0.1 Hz and rolls off at 6 db per octave. The sensor has a roll-off at 0.05 Hz. The data was corrected for the 0.1 Hz high pass filter, so it is band limited by the sensor roll-off.

A portable Refraction Technology 72A Data Acquisition Systems with 16 bit resolution was used to record the S-6000 seismometer at BE2U. The reftek recorder has a roll-off at 250 Hz and imposes an anti-aliasing filter at 40% of the sampling rate. We sampled the reftek data at 200 sps, so it has a band limit of 80 Hz. The S-6000 seismometer is flat to velocity to at least 100 Hz and rolls off at the low frequency end; it is down 3 db at 2 Hz and rolls off at 12 db per octave. We have corrected for this high pass filter, so that the response is effectively flat to DC.

Together, BE2D and BE2U have common data from 0.05 to 80 Hz. However, instrument and cultural noise further limit the effective frequency band of the data. Therefore the signal to noise ratios (SNR) were calculated and evaluated to determine the usable frequency band of the data recorded for each earthquake. This is reported below and usable frequency band are listed for each event in Table 1. The downhole ground motions were recorded as accelerations and were therefore integrated to velocities to be consistent with the uphole recordings.

Signal to Noise Ratios

For weak motion recordings, the noise in the signal is often the limiting factor for site response studies. The SNR for each earthquake in this study was calculated by estimating the spectral content of the first 20 to 30 seconds of the record (depending on the length of noise recorded prior to the earthquake signal) and a similar length of the earthquake signal. The two components of horizontal motion were combined into a complex signal as described by Steidl et al (1996). Fourier amplitude spectra of velocity records are used for the analysis. The Fourier signal amplitude spectrum was then divided by the Fourier noise spectrum for that earthquake. The SNR was calculated for the uphole and downhole recorded motions. A limiting SNR of 3:1 was chosen to determine the usable frequency band of each signal. Frequencies where the SNR was below 3 are believed to be

contaminated by the noise. The usable frequency bands for the uphole and downhole ground motions for each earthquake in this study are listed in Table 9.

Figure 3-20 show signal and noise for all the events. Examination of the noise and signal spectra for all 18 events in this study results in the following conclusions. The SNR for the uphole recordings was generally greater than 3 over a frequency range of 0.5 to 30 Hz. The downhole recordings had a much smaller usable frequency range with SNR equal to or above 3, from 1 to 8 Hz. However, the usable frequency range varies over the recorded earthquakes. The earthquakes with magnitudes greater than or equal to 3.0 tended to have a wider frequency band of high SNR.

One of the potential advantages to downhole instruments is the reduced cultural noise. Unfortunately for most of the recorded events in this study, instrument noise is more of a controlling factor. Because the YBI uphole and downhole instruments are different, the usable frequency band is also different for each instrument. The downhole Wilcoxon 731s 10v/g accelerometer can be limited by noise at low frequencies, generally below 1 Hz, except for the larger events in the study where the SNR is greater than 3 down to 0.3 Hz. On the other hand, the uphole S-6000 seismometer is less limited at the low frequencies down to 0.2 Hz in some cases but can be limited at high frequencies for small amplitude events. In particular, the S-6000 has a significant increase in noise for frequencies above 30 Hz. The Wilcoxon instrument has less instrument noise at the higher frequencies and therefore results in a higher SNR above 10 Hz than the downhole instrument. So unfortunately for this uphole/downhole pair, the uphole instrument is limited by noise for high frequencies and the downhole instrument is limited at low frequencies when recording weak motion. Both instruments have high SNR for the larger earthquakes.

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Acknowledgments

This work was funded by Caltrans, contract no. 59A0238. Instrumentation was been made possible by the personnel support of, Caltrans, Sacramento, California, in particular: Pat Hipley, Lalliana Mualchin, Reid Buell, John Bowman, Mark Palmer, Kathy Amaru, James Dent, and Robert Fletcher. Extensive instrument financial support was contributed by UCB, LBL, LLNL-LDRD, U.C. Campus/Laboratory Collaboration (CLC) program, and USGS. This would not have been possible without the generous contribution of temporary recording instrument provided by the LLNL Seismic Observatory and LBL Instrumentation Program.

This work was performed under the auspices of the U.S. Department of Energy by the University of California, Lawrence Livermore National Laboratory under contract No. W-7405-Eng-48.

Table 1: Dumbarton Bridge Recording sites

i.d.	sensors	latitude	longitude	depth (m)	sensor h1, h2 + 090	Recording
<u>Pier 01</u> DWA, DWS DWN DWB	S-13 Wil-731-200, HS-1 Wil-731-200, HS-1 HS-1, HS-1	37.49947	122.12755	00.0 m, abut. 01.5, Pier 01 71.6, " 228.0, "	N320°E 000° --- 033°	07/94 - 09/94 09/94 - 09/94 09/94 - 09/94 08/93 - present
<u>Pier 27</u> DMB CAP	Wil-731,HS-1 Wil-731-200, HS-1	37.50687 37.517	122.11566 122.104	189.2, Pier 27 pile cap, Pier 27	N020°E	07/94 - present 07/92 - 11/92
<u>Pier 44</u> DES DEM DEB	Wil-731-200, HS-1 Wil-731-200,HS-1 Wil-731, HS-1	37.51295	122.10857	01.5, Pier 44 62.5 157.9	N000°E ---- 097°	11/94 - 09/94 09/94 - 09/94 07/94 - present

Table 2: Bay Bridge Recording sites

i.d.	sensors	latitude	longitude	depth (m)	sensor h1, h2 + 090	Recording
SFA	S-6000	37.7861	122.3893	00.0 m,	N143°E	6/98-present
BBW2	Wil-731A,HS-1	37.79120	122.38525	57.6	N042°E	4/96-present
BBW5	Wil-731A,HS-1	37.8010	122.3737	36.3	N142°E	1/97-present
YBA	Wil-731A,HS-1	37.8094	122.3645	3.0	N150°E	6/98-present
BE2U	S-6000	37.81427	122.35815	0.00	N220°E	7/96-present
BE2D (YBIB)	Wil-731A,HS-1	37.81427	122.35815	60.96	N165°E	7/96-present
BE07	Wil-731A,HS-1	37.81847	122.34688	134.0	N117°E	2/96-present
BE17	Wil-731A,HS-1	37.82086	122.33534	160.0	N168°E	8/95-present
BE23	HS-1	37.82167	122.32867	150	N---°E	3/94-10/95

Table 3: San Rafael Bridge Recording sites

i.d.	sensors	latitude	longitude	depth	sensor h1, h2 + 090	Recording
P34	Wil-731A,HS-1	37.93583	122.44540	109.0 m		8/97-present
P58	Wil-731A,HS-1	37.93372	122.41313	44.0 m	N0°E	6/97-present

Table 4: San Mateo Bridge Recording sites

i.d.	sensors	latitude	longitude	depth	sensor h1, h2 + 090	Recording
P343	Wil-731A,HS-1	37.59403	122.23242	298.0 m	N0°E	not recorded

Table 5: Carquinez Bridge Recording sites

i.d.	sensors	latitude	longitude	depth	sensor h1, h2 + 090	Recording
CRQB	Wil-731A,HS-1	38.05591	122.22402	-----	N0°E	6/98-present

Table 6: Sensor Orientation Calculations, Bay Bridge

Orientations of up on channel 2; ch3 = ch2 + 090; Channel 1 is vertical, positive down, except **	SFA**	BBW2	BBW5	YBA**	BE2D	BE2U	BE07	BE17	BE23
9812041216	N143E	N042E	N142E	N150E	N165E	N310E	N117E	N168E	
+prior 08/24/99 since 08/24/99	N131E N136E								
*prior 01/15/97 since 01/15/97						N143E N310E			
Vertical									
vertical: up on channel-1	UU	DD	DD	DD	DD	UU	DD	DD	

Table 7: Events recorded by Bay Bridge Network

Earthquake	Time	Latitude	Longitude	Depth	Mag	Fault
2000/02/29	10:48:00.58	37.7980	-121.9428	15.94	2.05	Calaveras
2000/02/29	11:10:09.72	37.8682	-122.2392	10.52	2.15	Hayward
2000/03/02	09:22:12.21	37.2578	-121.6400	6.01	1.45	Calaveras
2000/03/28	21:03:07.27	37.6330	-122.0203	6.04	3.04	San Andreas
2000/04/03	06:08:35.89	37.4342	-121.7775	9.00	1.56	Calaveras
2000/04/06	19:03:06.54	38.3492	-122.1980	8.04	2.61	Hayward
2000/04/09	21:25:22.16	38.0880	-122.4033	13.31	2.40	San Andreas
2000/04/10	13:05:29.64	37.4747	-121.7150	9.70	3.20	Calaveras
2000/04/11	14:12:15.93	37.8447	-122.0097	14.87	2.52	Calaveras
2000/04/14	12:22:31.77	37.9830	-122.0433	15.76	3.19	Calaveras
2000/04/14	17:49:25.62	37.6038	-121.9708	9.89	3.04	Calaveras
2000/04/24	08:03:51.47	37.4018	-121.7267	5.45	1.24	Calaveras
2000/04/29	06:04:49.01	37.7378	-122.5512	7.22	2.51	San Andreas
2000/05/02	10:14:45.67	37.9222	-122.2905	6.54	2.19	San Andreas
2000/05/03	22:05:11.80	37.7277	-122.1177	8.46	2.28	Hayward
2000/05/14	14:11:49.05	37.3338	-122.0613	4.06	2.39	Hayward
2000/05/21	05:07:02.82	37.7737	-122.5888	6.62	2.13	San Andreas
2000/05/23	12:35:06.85	37.7113	-122.1062	6.04	2.60	Hayward
2000/05/25	06:43:08.73	37.8652	-122.2380	9.59	1.88	Hayward
2000/05/26	06:21:15.74	37.9898	-122.1818	9.10	2.17	Hayward
2000/05/26	14:23:20.40	37.9517	-122.7218	7.67	2.28	San Andreas
2000/05/28	04:30:06.37	37.5677	-122.4317	10.11	1.21	San Andreas
2000/05/30	02:10:58.51	37.3072	-122.0778	4.97	2.58	Hayward
2000/05/30	08:10:41.59	37.3482	-121.7230	9.82	1.25	Hayward
2000/06/02	10:17:24.38	37.7512	-122.1512	5.71	2.65	Hayward
2000/06/08	05:53:27.89	37.2958	-121.6752	5.11	2.20	Hayward

Earthquake	Time	Latitude	Longitude	Depth	Mag	Fault
2000/06/13	11:48:11.55	37.3105	-121.6805	7.51	3.47	Hayward
2000/06/17	00:52:09.94	37.7203	-122.5725	3.28	2.02	San Andreas
2000/06/18	11:13:26.28	37.7652	-121.9290	14.25	0.81	Calaveras
2000/06/18	17:16:07.64	37.9095	-122.2938	3.42	1.33	Hayward
2000/06/25	07:23:18.26	37.1240	-121.5265	7.83	3.63	Calaveras
2000/06/25	16:03:21.39	37.7318	-122.5395	5.96	1.14	San Andreas
2000/06/25	16:04:35.30	37.7337	-122.5397	5.75	1.56	San Andreas
2000/07/03	22:13:18.06	37.3420	-121.7055	8.55	3.33	Hayward
2000/07/04	10:08:13.43	37.8030	-122.0227	8.82	1.75	Hayward
2000/07/07	12:08:22.35	37.7160	-122.5442	10.33	1.58	San Andreas
2000/07/09	14:43:47.46	37.8035	-122.1823	8.38	1.77	Hayward
2000/07/11	23:40:20.68	37.1282	-121.5302	7.46	2.32	Hayward
2000/07/14	11:23:16.39	38.0688	-122.2405	7.63	1.97	Hayward
2000/07/15	07:29:20.47	37.8893	-122.2603	4.72	1.07	Hayward
2000/07/15	11:56:38.97	37.9752	-122.0335	15.43	3.61	Hayward
2000/07/18	02:02:01.45	37.6095	-122.4752	8.33	1.83	San Andreas
2000/07/31	03:01:07.83	37.4185	-121.7667	7.76	2.25	Calaveras
2000/08/22	10:00:57.97	38.4065	-122.1558	3.64	0.62	Hayward
2000/09/02	08:00:30.44	37.9887	-122.0557	15.63	2.35	Calaveras
2000/09/02	21:58:47.87	37.9877	-122.0538	16.23	2.51	Calaveras
2000/09/03	08:36:30.09	38.3788	-122.4127	10.21	5.17	Hayward
2000/09/03	09:11:15.97	38.3922	-122.4032	6.10	1.64	Hayward
2000/09/03	21:00:03.07	38.3648	-122.3998	8.58	2.31	Hayward
2000/09/09	03:02:16.36	37.6513	-122.0443	5.23	2.03	Hayward
2000/09/10	12:37:19.34	38.3817	-122.4088	7.13	2.55	Hayward
2000/09/12	06:55:26.17	37.5533	-121.6765	5.18	2.49	Calaveras
2000/09/18	22:31:47.99	37.9173	-122.3017	1.56	1.08	Hayward

Earthquake	Time	Latitude	Longitude	Depth	Mag	Fault
2000/09/23	23:16:52.87	37.8937	-122.2188	7.55	2.14	Hayward
2000/09/24	22:27:46.52	37.8773	-122.2313	10.02	1.53	Hayward
2000/09/27	10:18:55.23	37.8500	-122.2325	6.07	2.26	Hayward
2000/09/28	08:44:06.49	37.3593	-121.7262	6.96	2.48	Hayward
2000/10/03	11:30:54.65	37.6400	-122.4945	8.09	1.99	San Andreas
2000/10/27	05:47:56.59	37.7603	-122.1677	6.01	2.28	Hayward
2000/10/30	20:33:56.72	37.6695	-122.4938	11.80	2.06	San Andreas
2000/11/12	17:49:56.34	37.9705	-122.3407	6.89	2.55	Hayward

Table 8: Events recorded at each station.

Earthquake	BBW2	BBW5	BE07	BE17	BE23	SFA	YBA
0002291048					X		
0002291110			X		X		
0003020922						X	
0003282103	X	X			X		
0004030608						X	
0004061903							X
0004092125					X		
0004101305					X		
0004111412			X		X		
0004141222		X	X	X	X		
0004141749	X	X	X	X	X		
0004240803						X	
0004290604	X		X	X	X		
0005021014	X		X	X	X	X	
0005032205					X		
0005141411					X		
0005210507					X		
0005231235	X		X	X	X		
0005250643			X	X	X		
0005260621			X		X		
0005261423					X		
0005280430					X		
0005300210					X		
0005300810						X	
0006021017	X		X	X	X		
0006080553					X		

Earthquake	BBW2	BBW5	BE07	BE17	BE23	SFA	YBA
0006131148	X				X		
0006170052					X		
0006181113						X	
0006181716					X		
0006250723	X			X	X		
0006251604					X		
0007032213					X		
0007041008					X		
0007071208					X		
0007091443					X		
0007112340					X		
0007141123					X		
0007150729					X		
0007151156	X			X	X		
0007180202					X		
0007310301					X		
0008221000						X	
0009020800				X			
0009022158				X			
0009030836	X			X		X	
0009030911	X						
0009032100	X						
0009090302					X		
0009101237					X		
0009120655					X		
0009182231					X		
0009232316				X	X		

Earthquake	BBW2	BBW5	BE07	BE17	BE23	SFA	YBA
0009242227					X		
0009271018				X	X		
0009280844					X		
0010031130					X		
0010270547				X			
0010302033				X			
0011121749				X			

San Francisco Bay Bridges

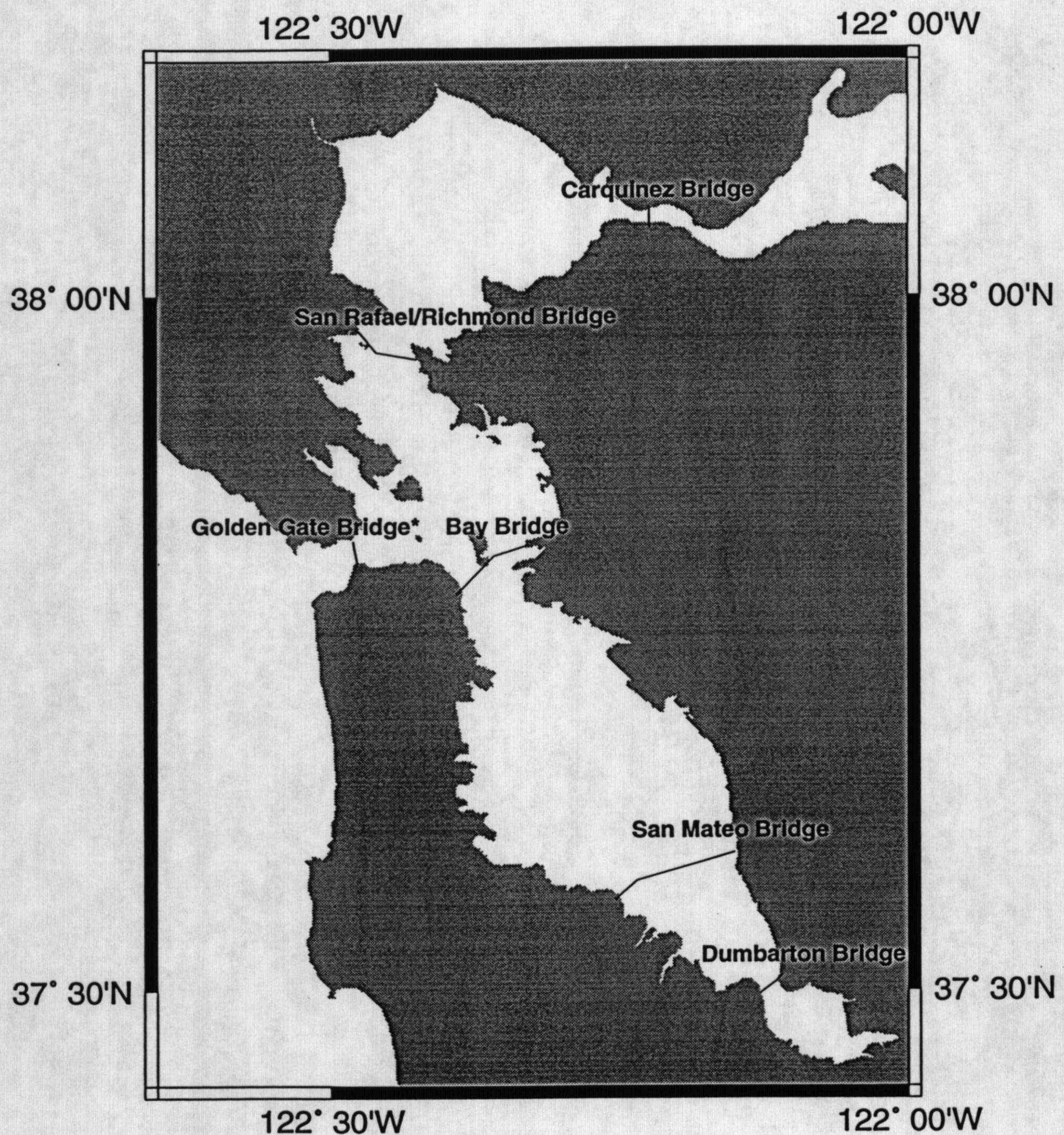
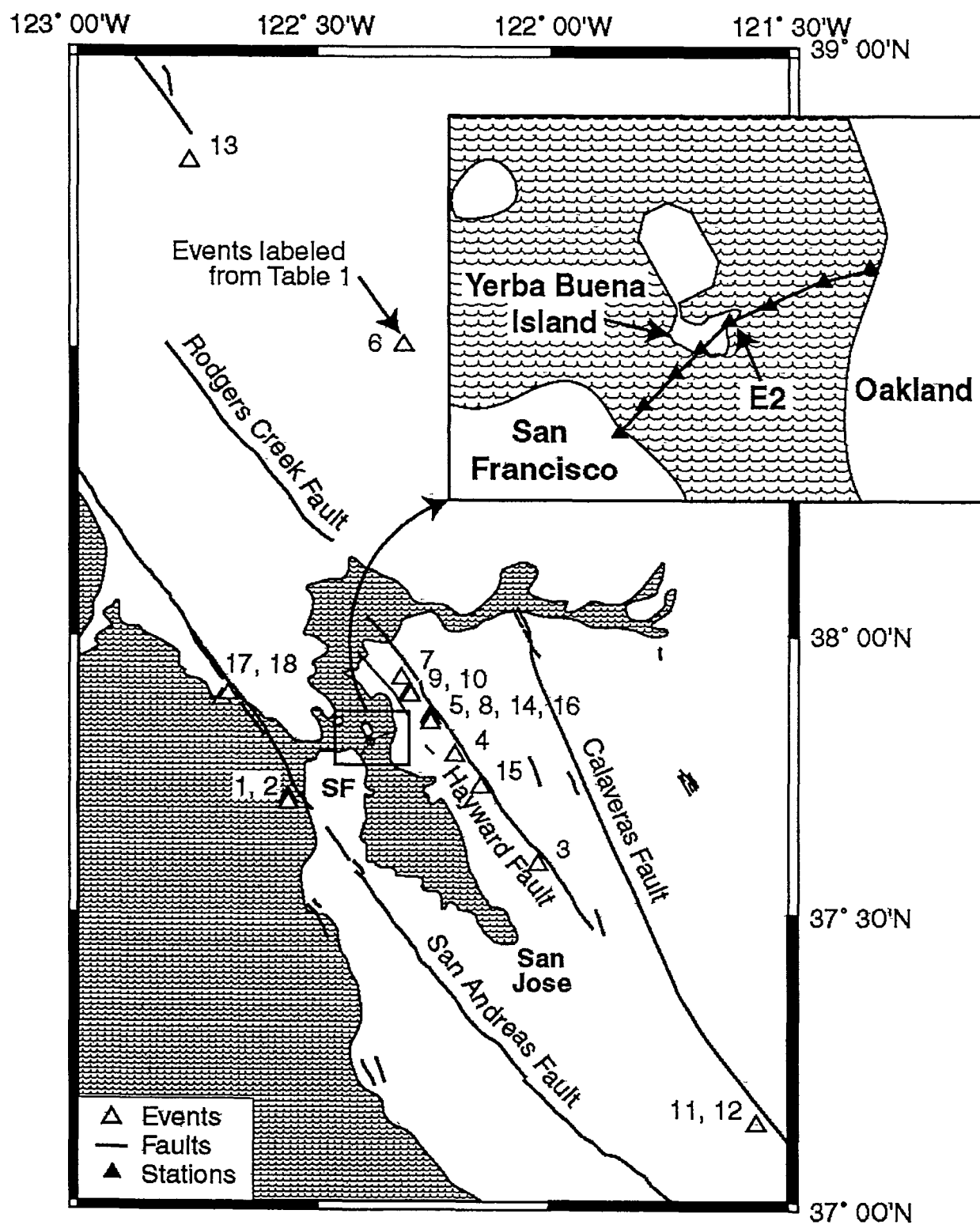
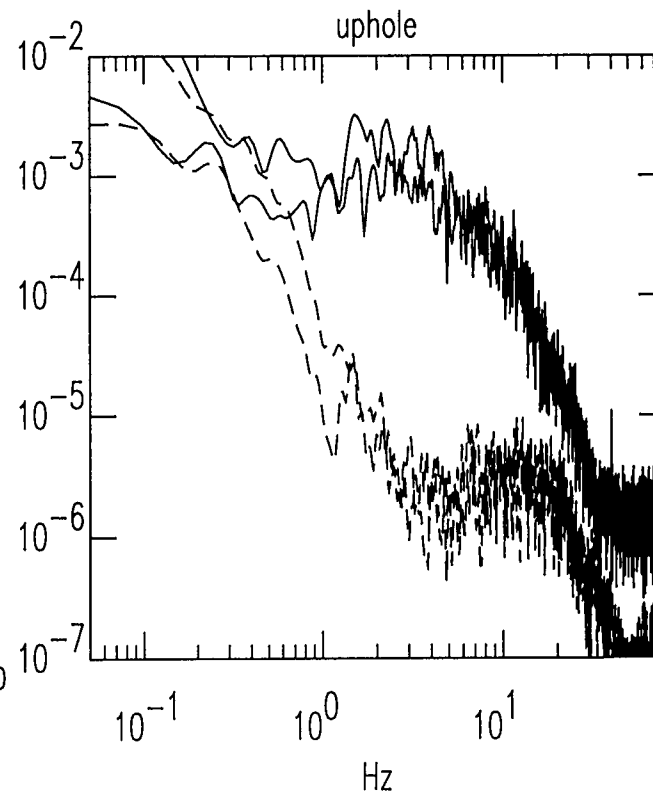
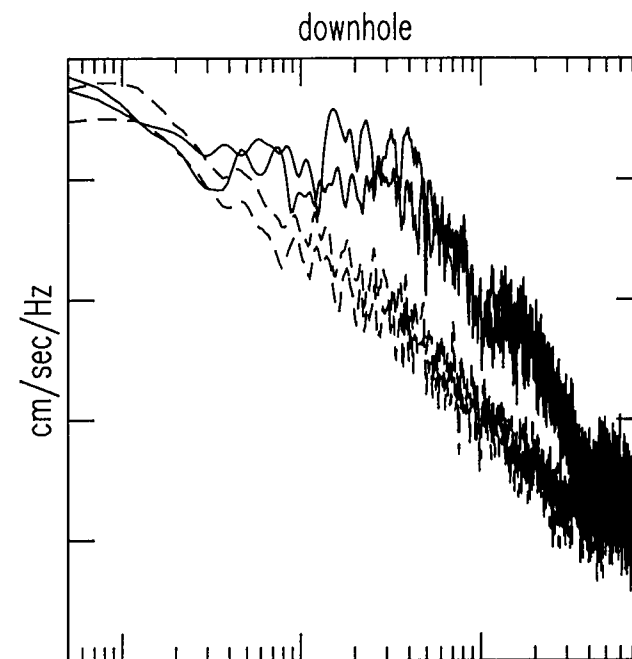
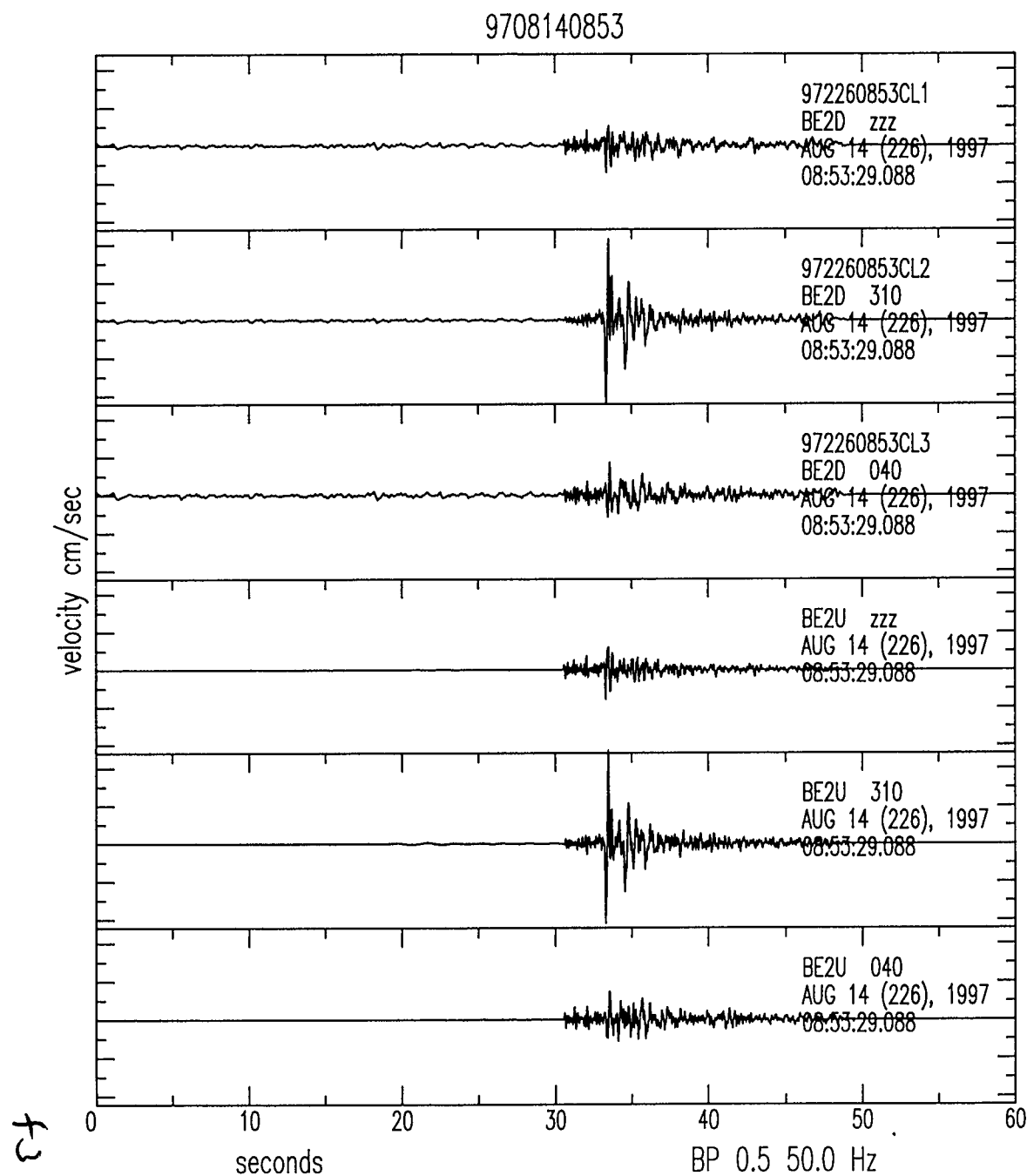
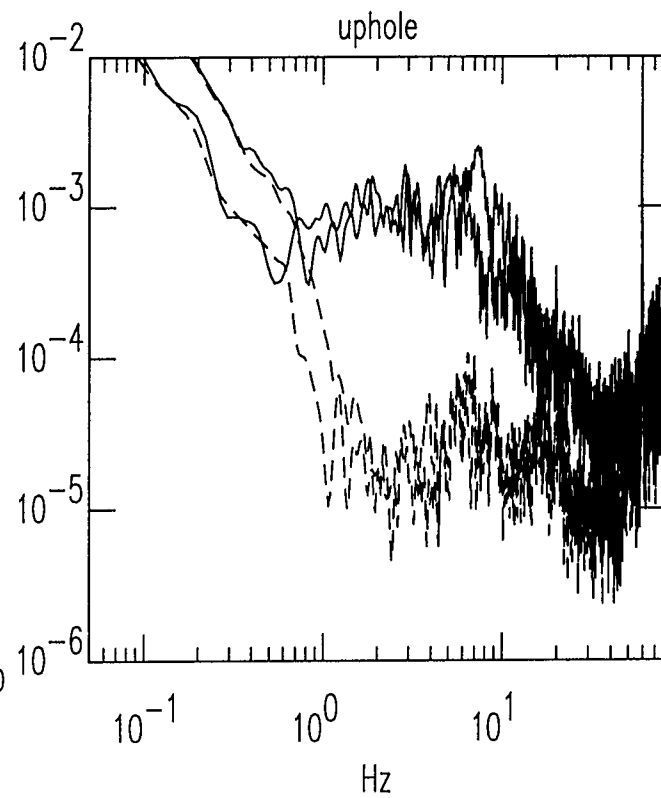
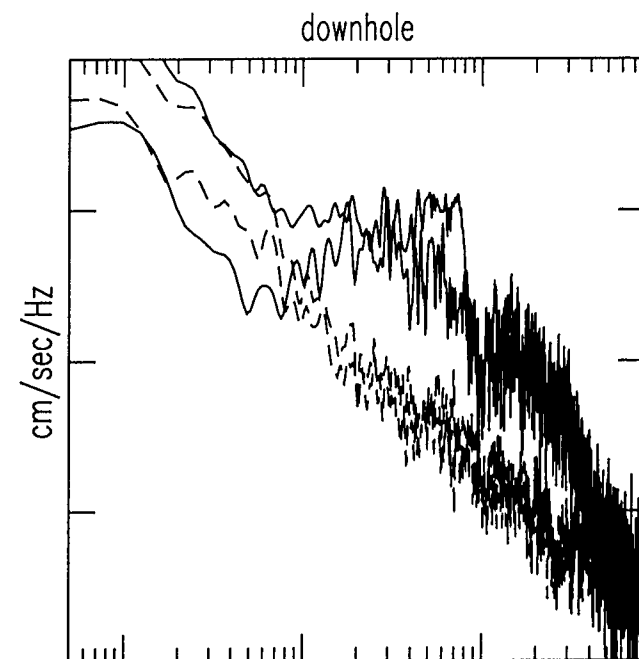
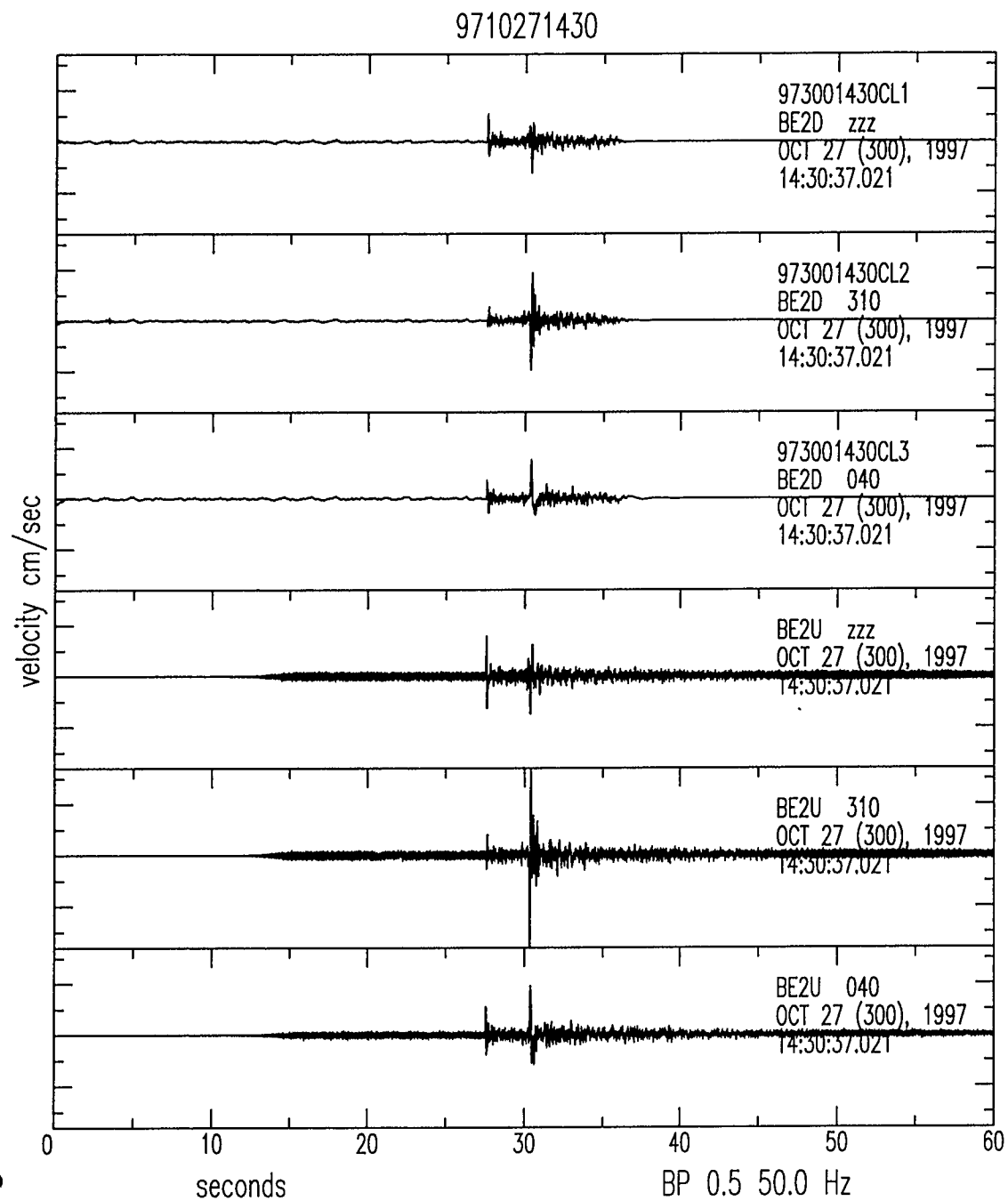


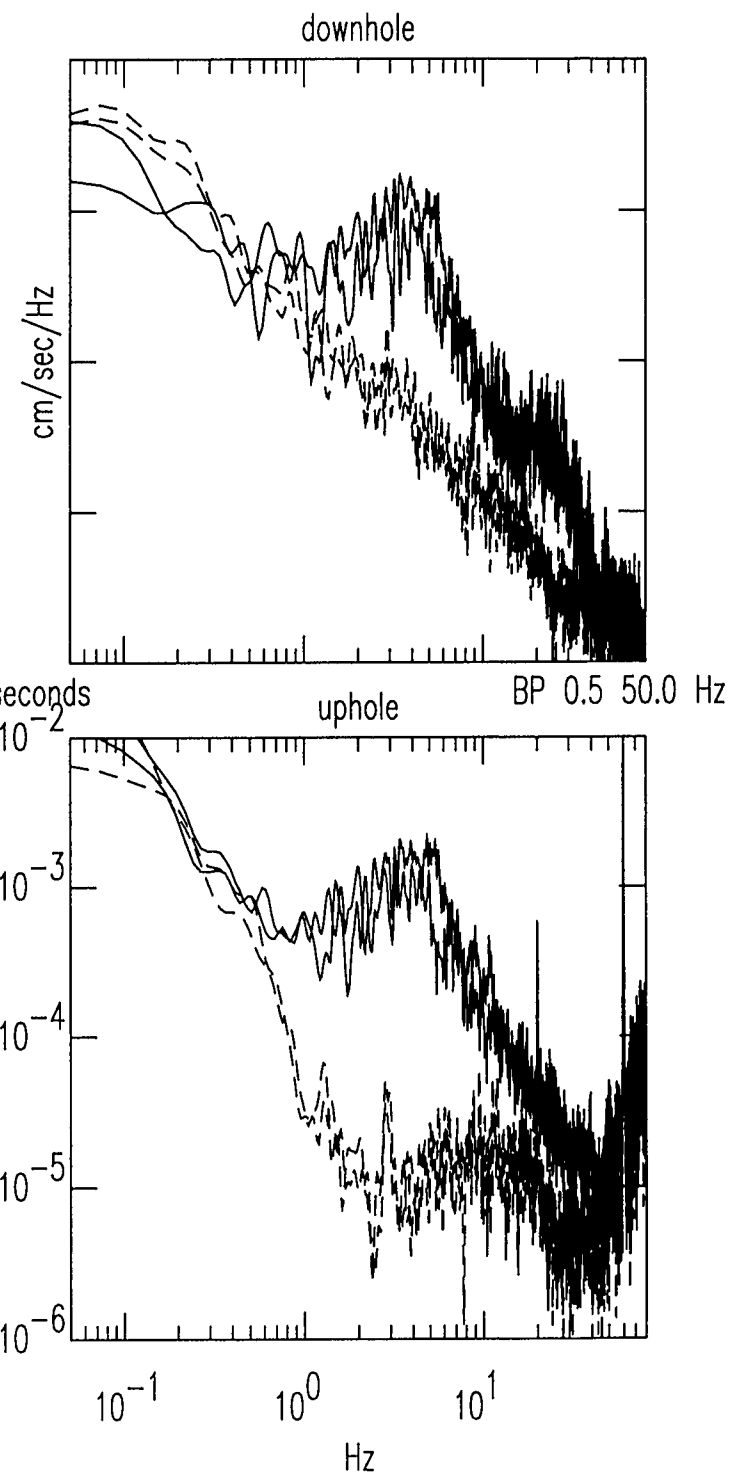
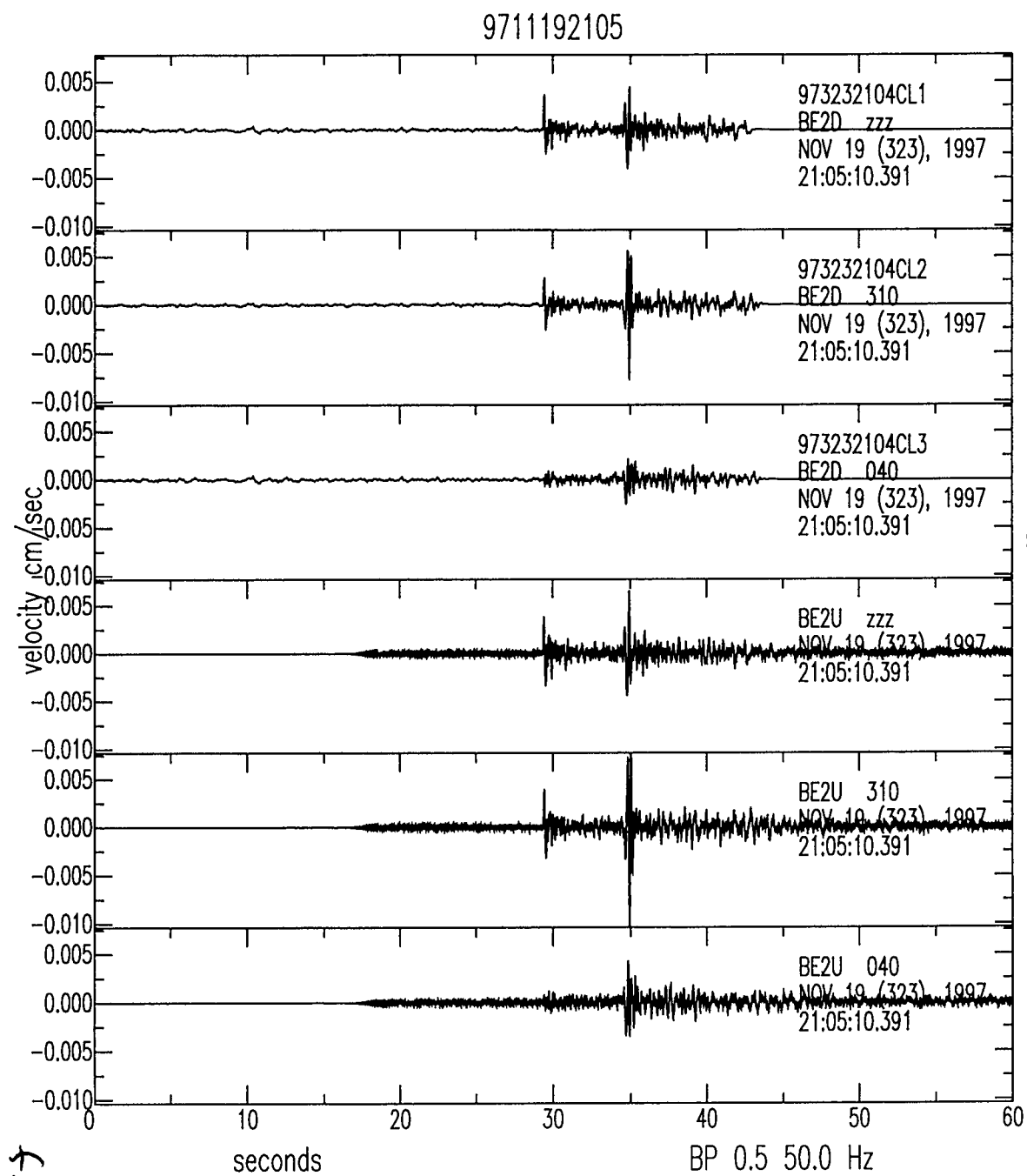
Figure 1: Map of the San Francisco Bay. (*Bridge not used in the bridge network study.)





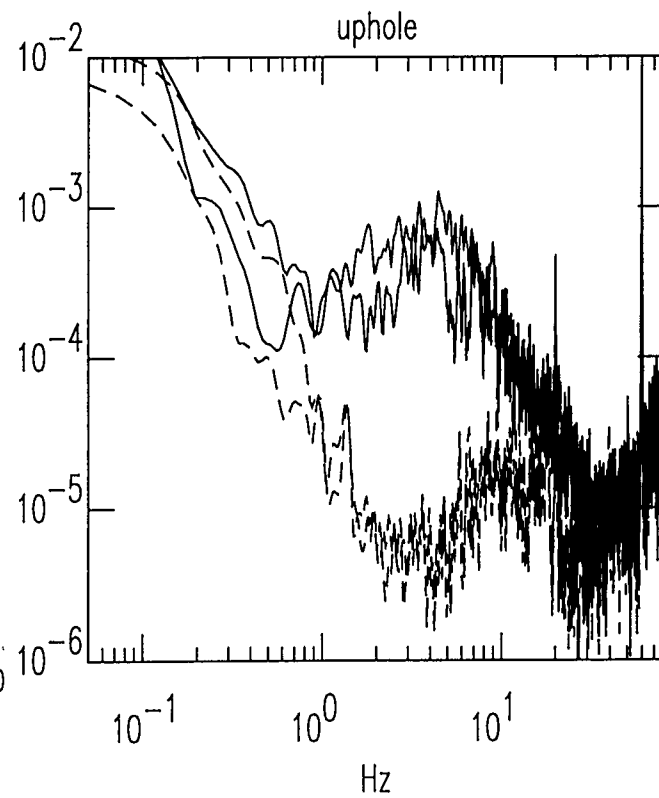
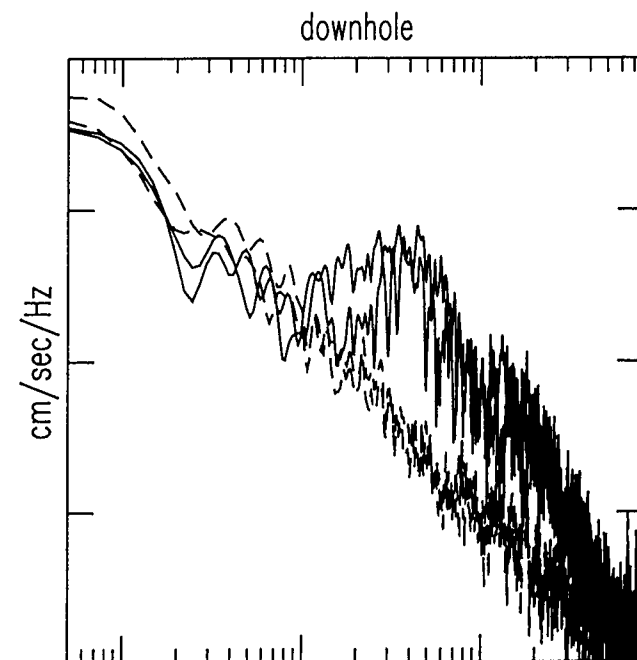
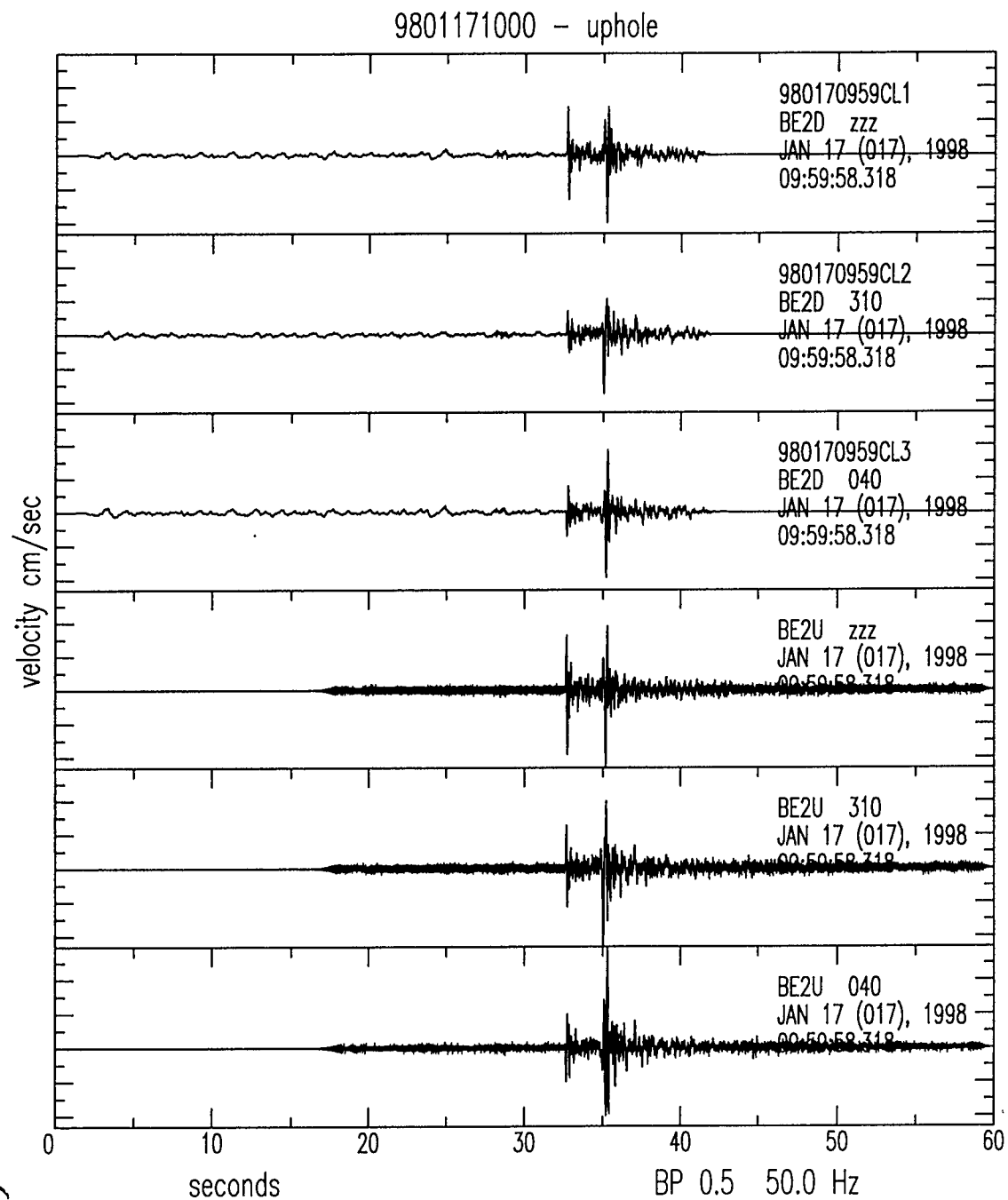
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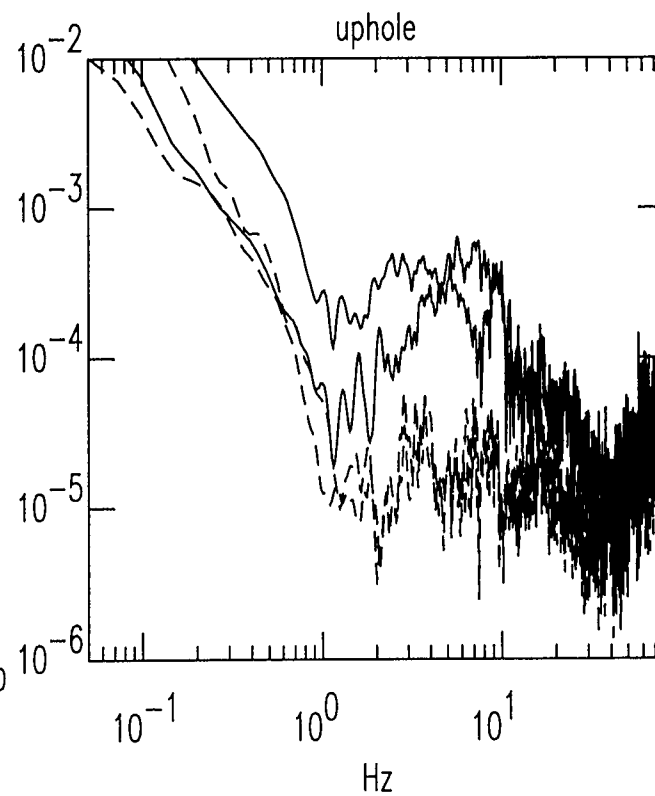
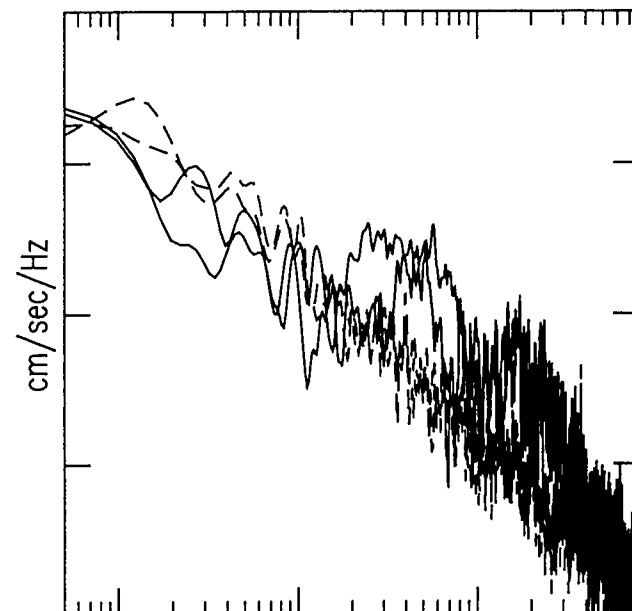
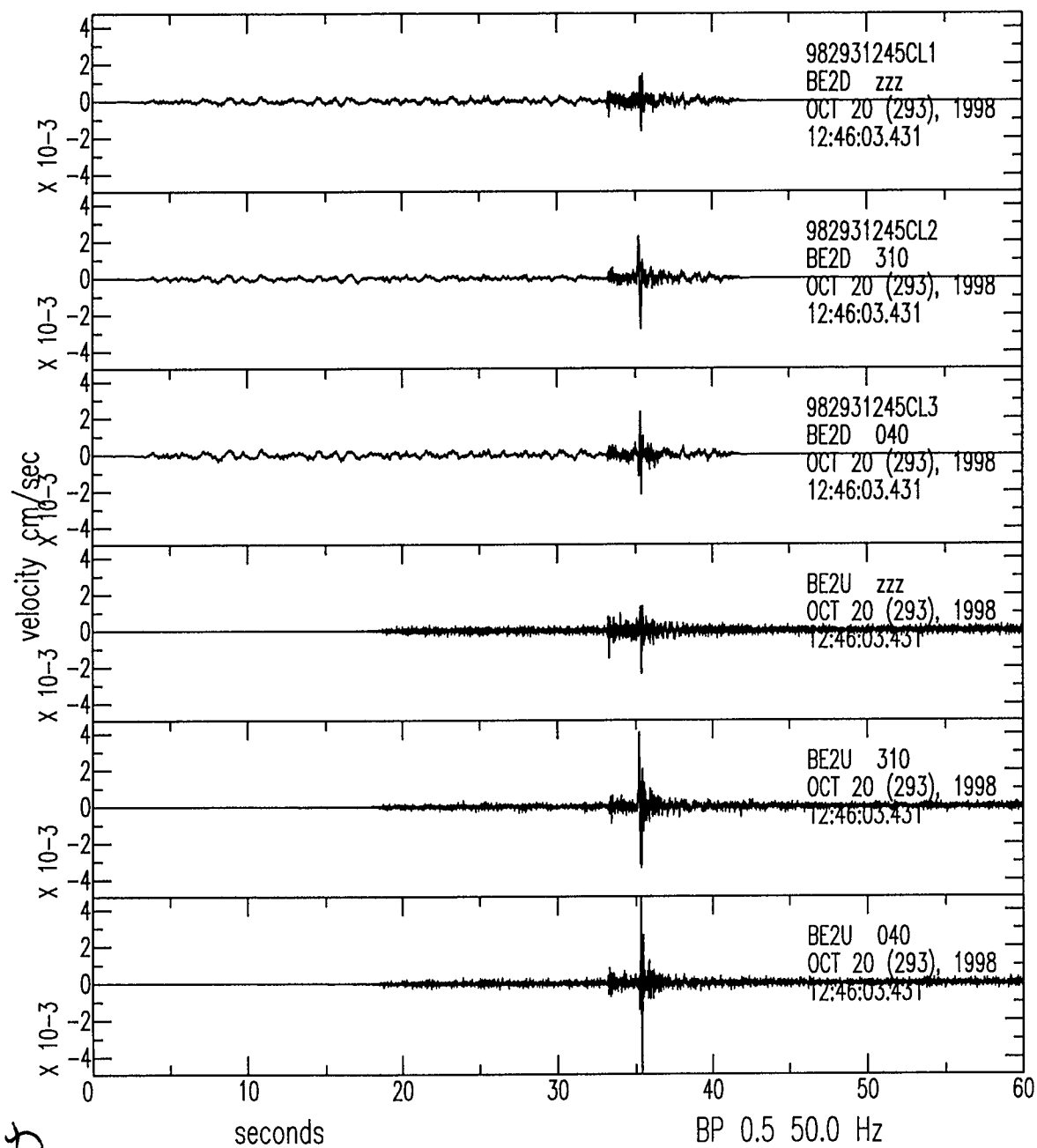


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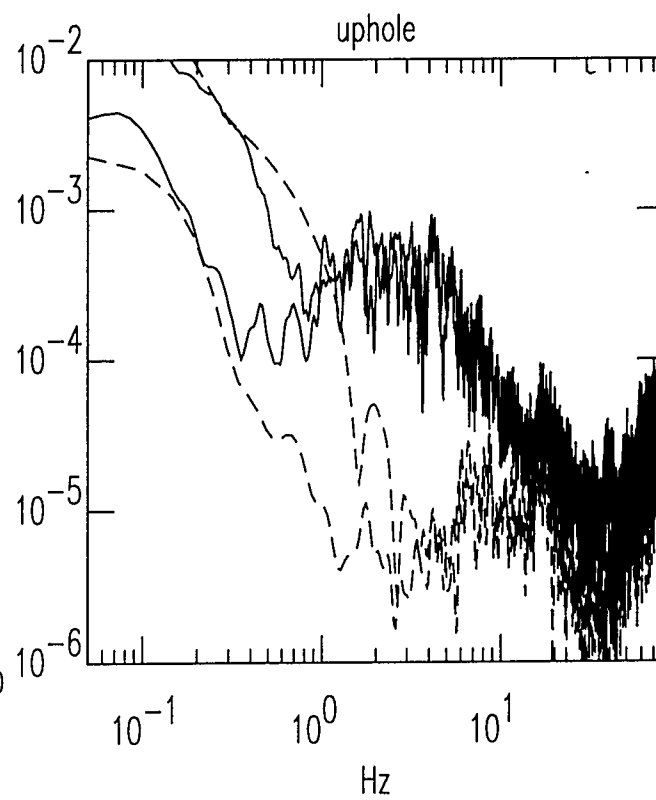
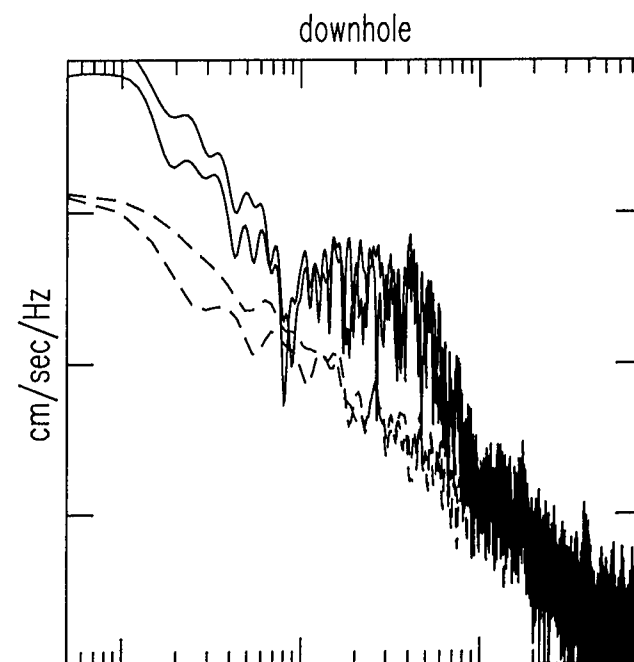
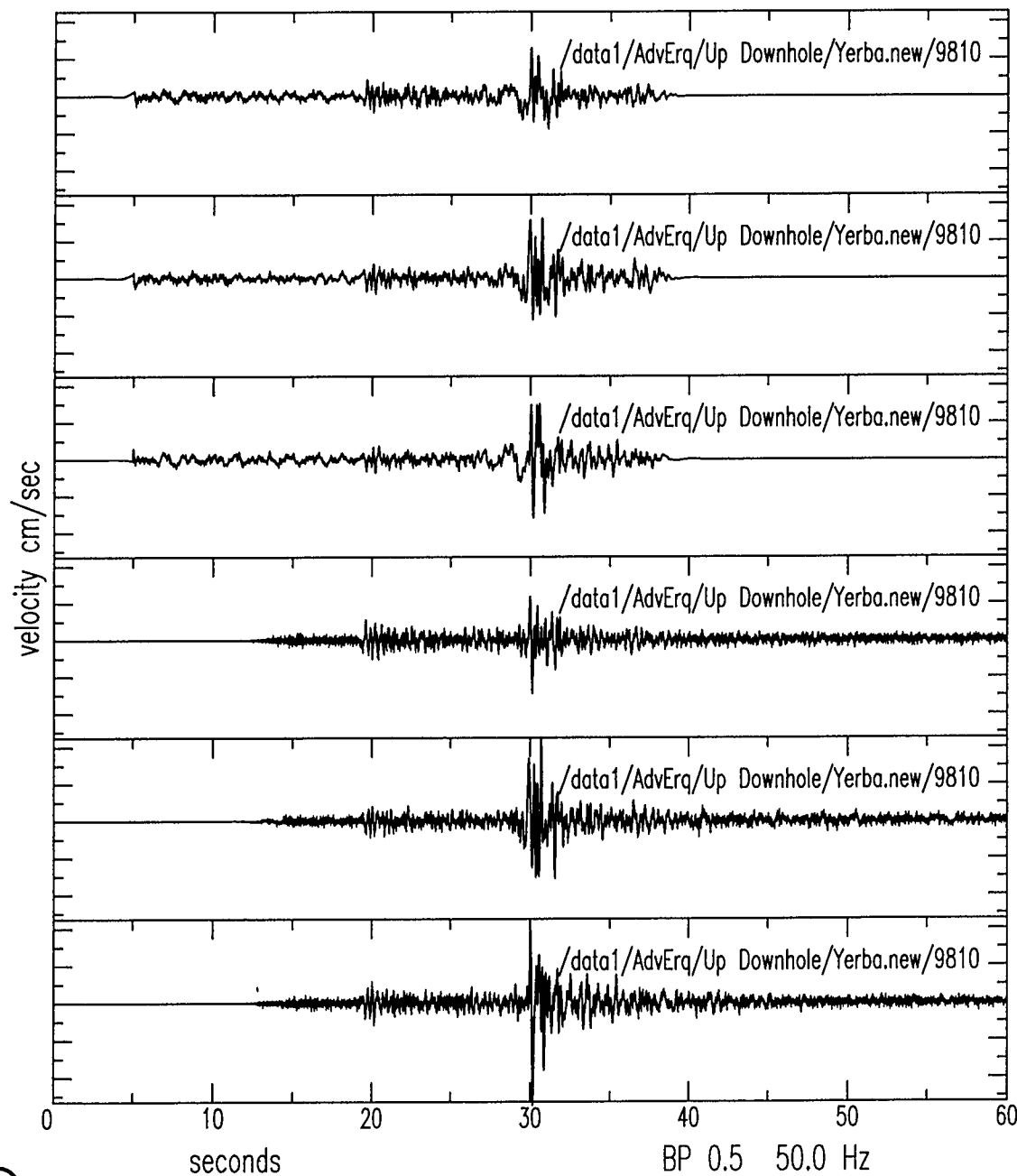
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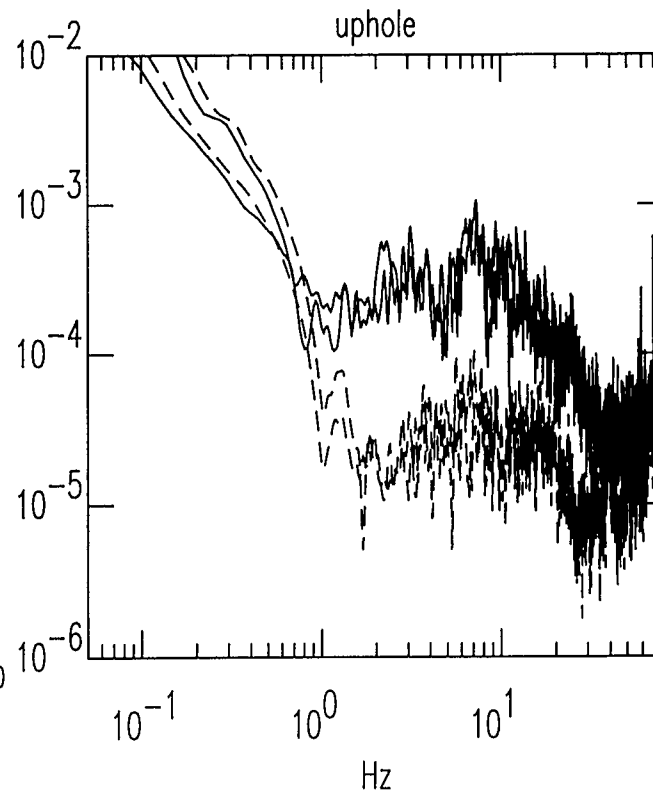
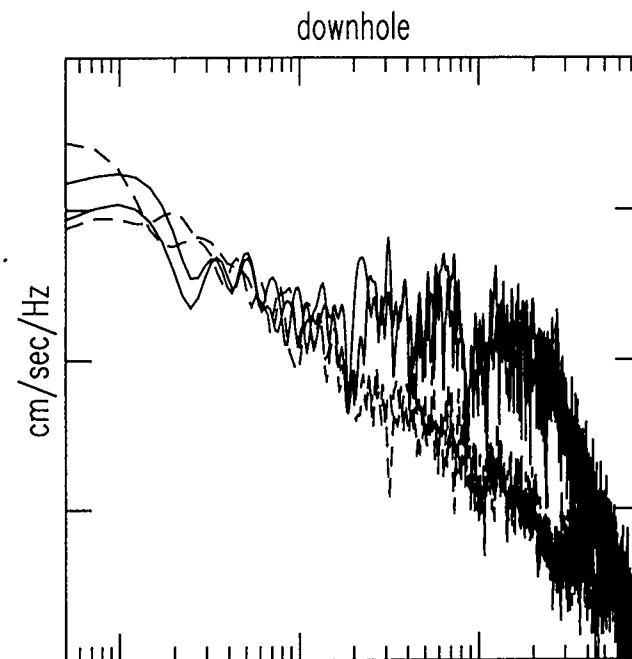
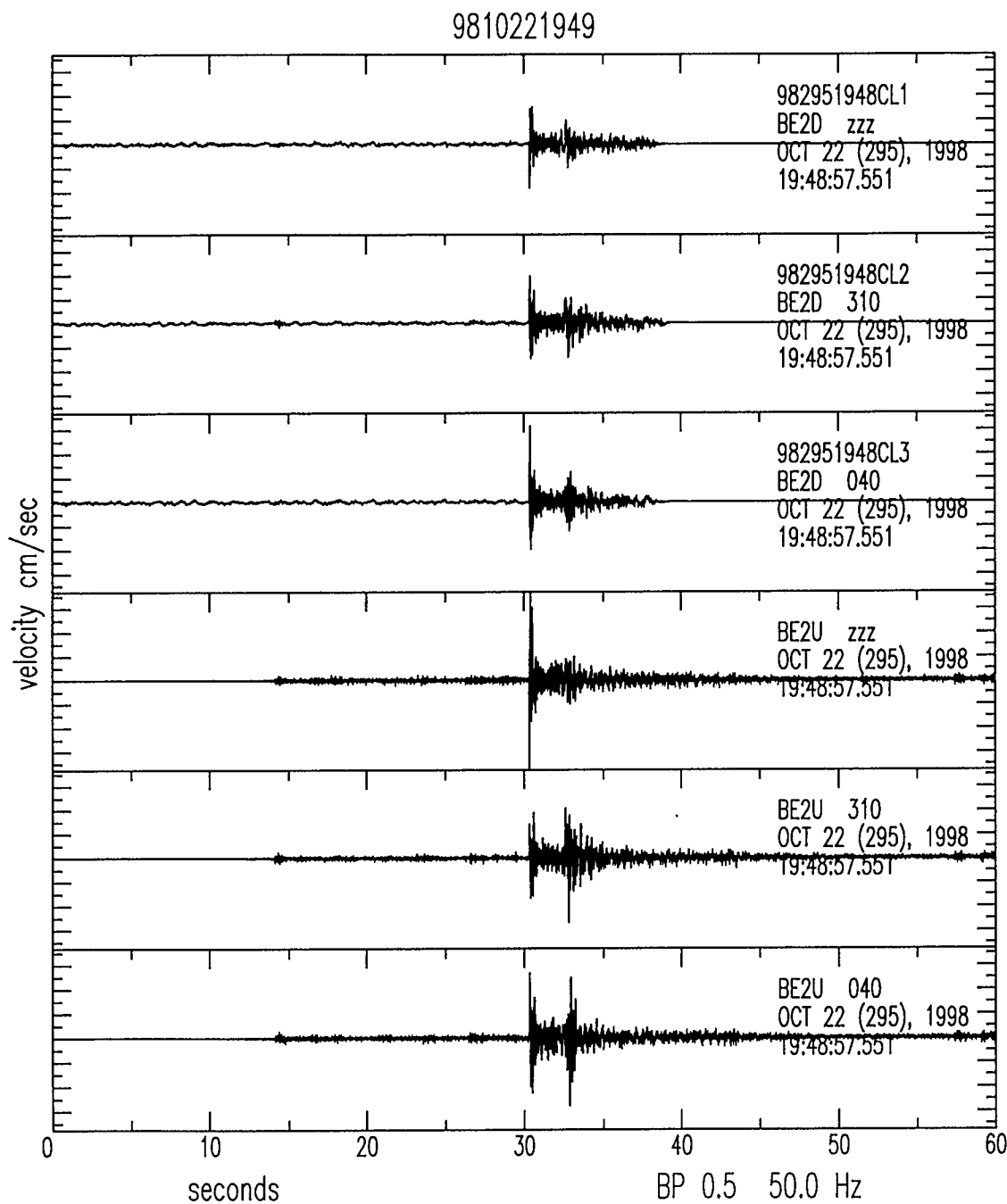


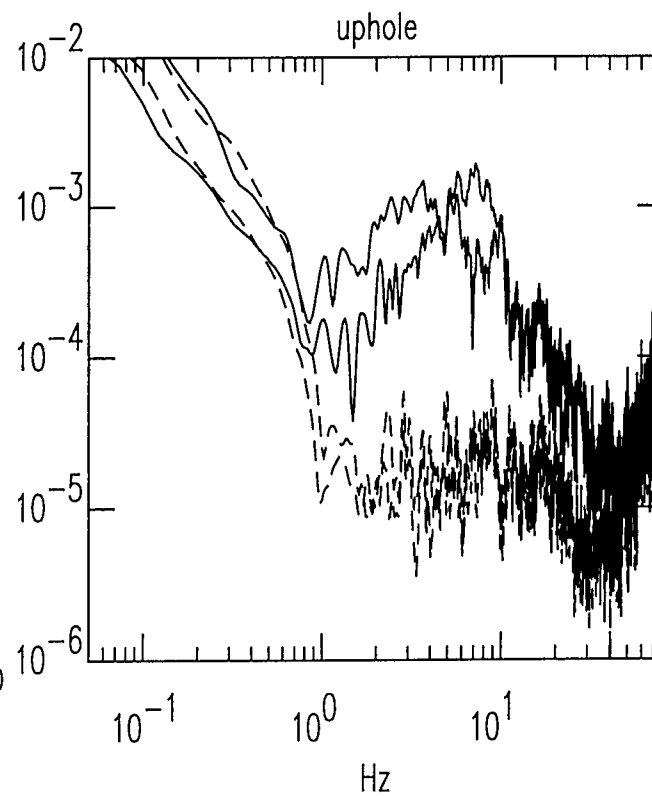
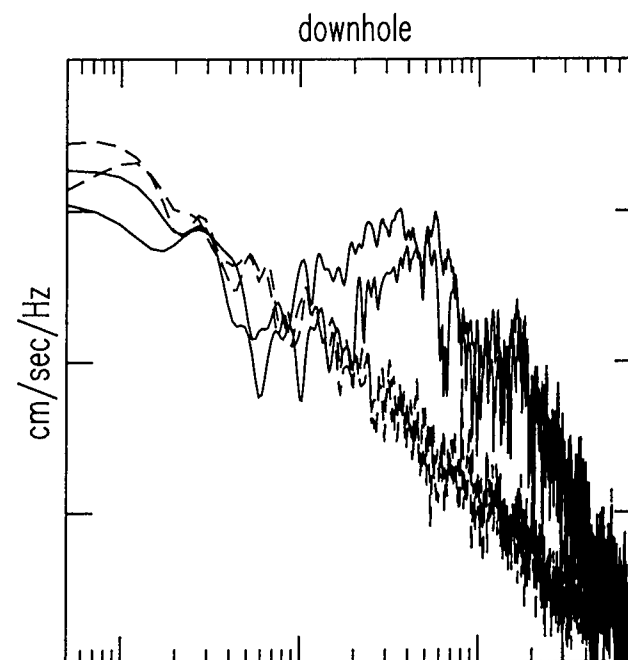
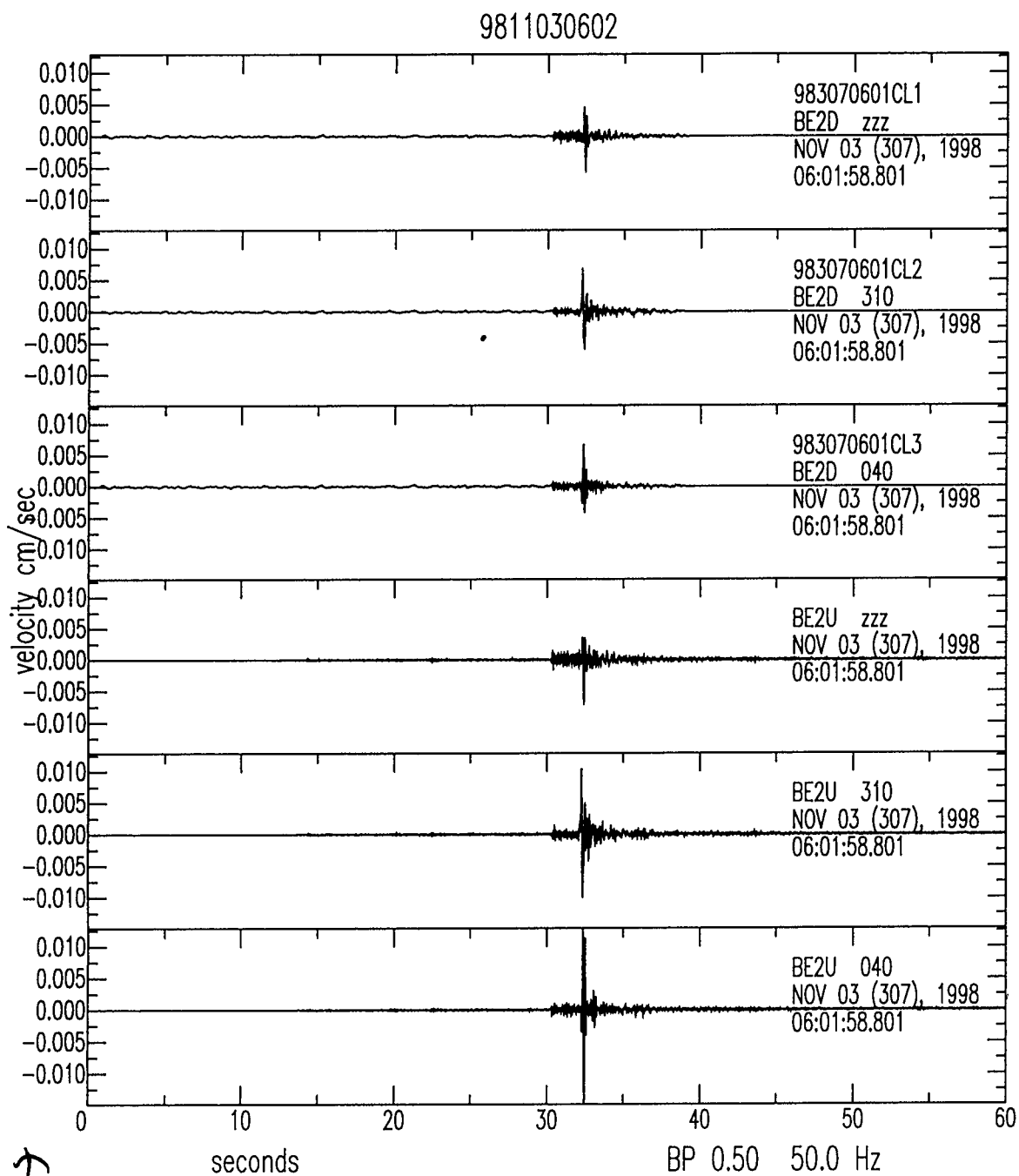
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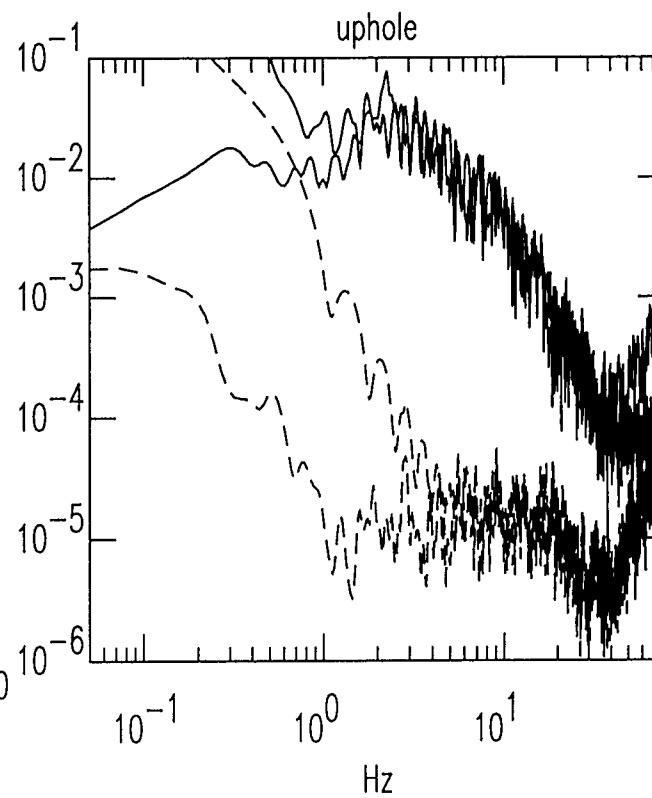
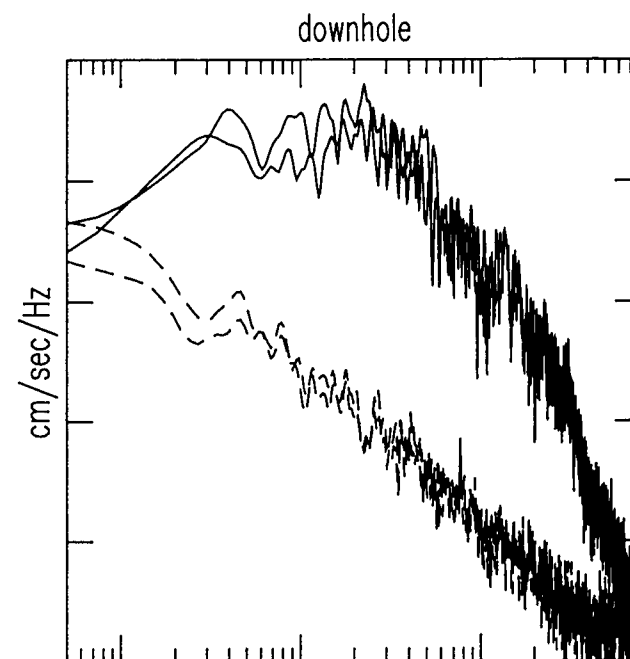
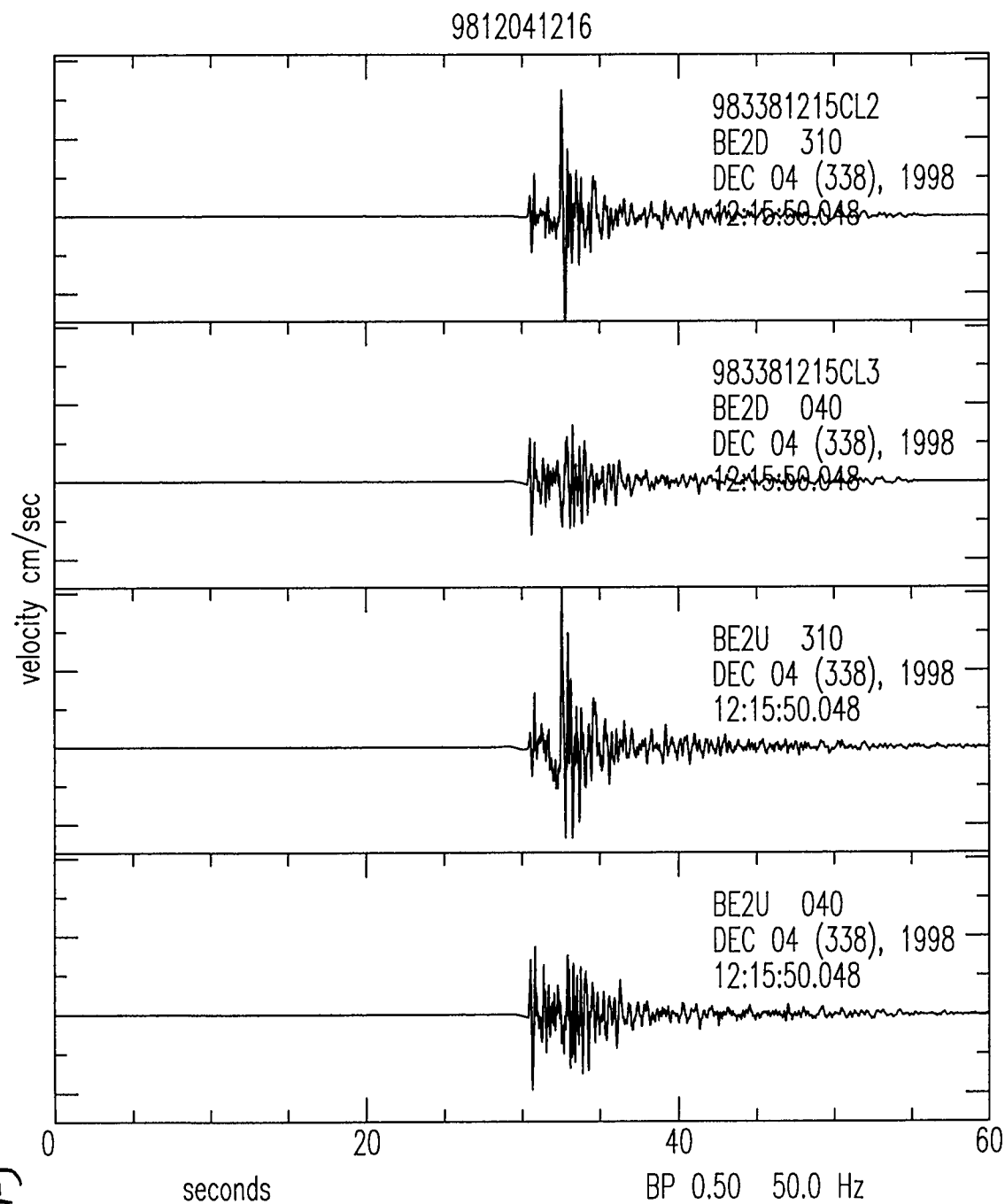
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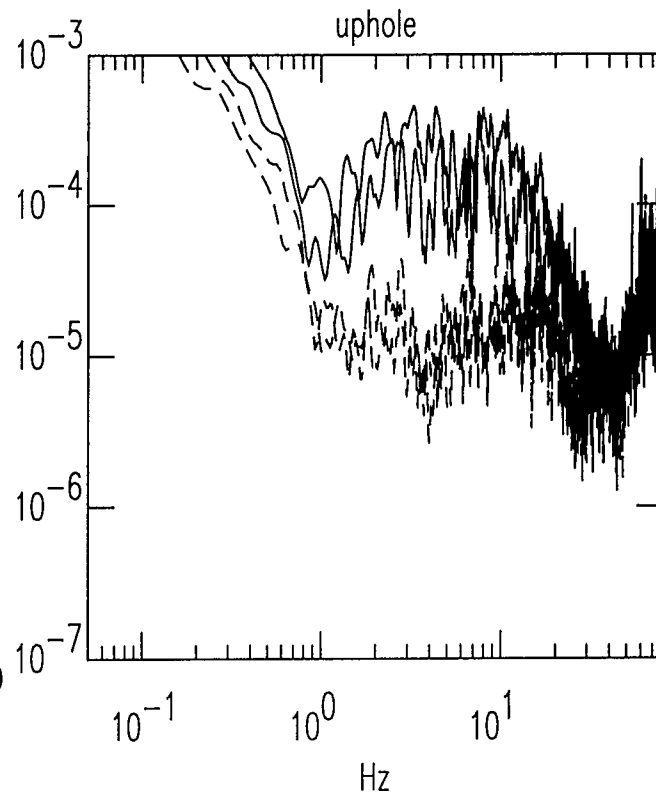
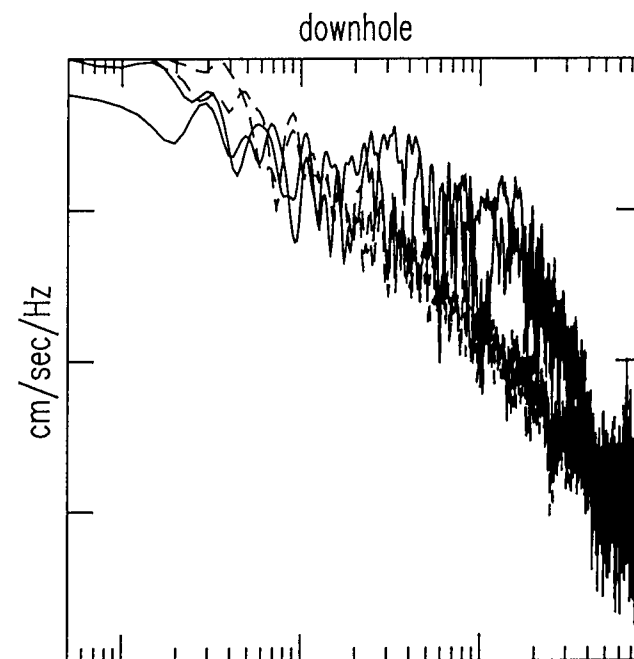
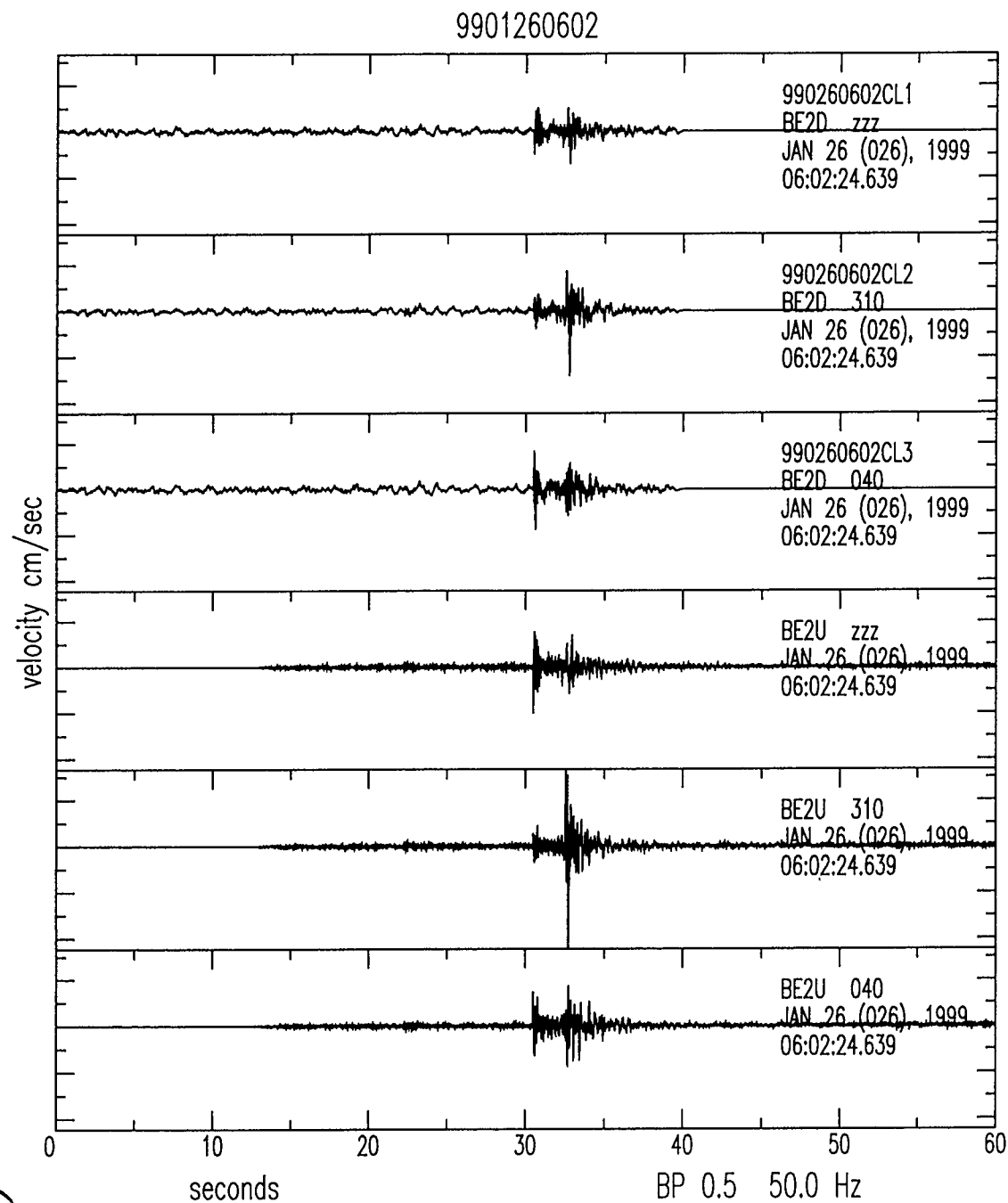


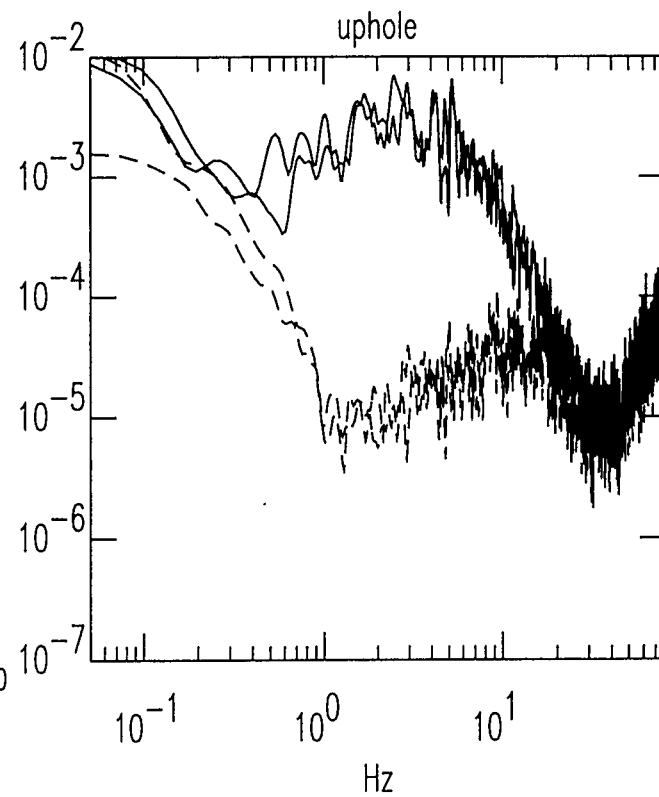
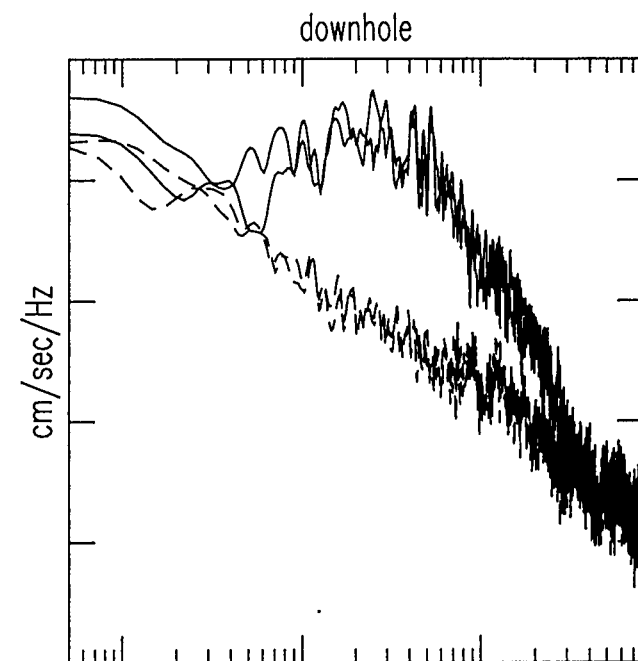
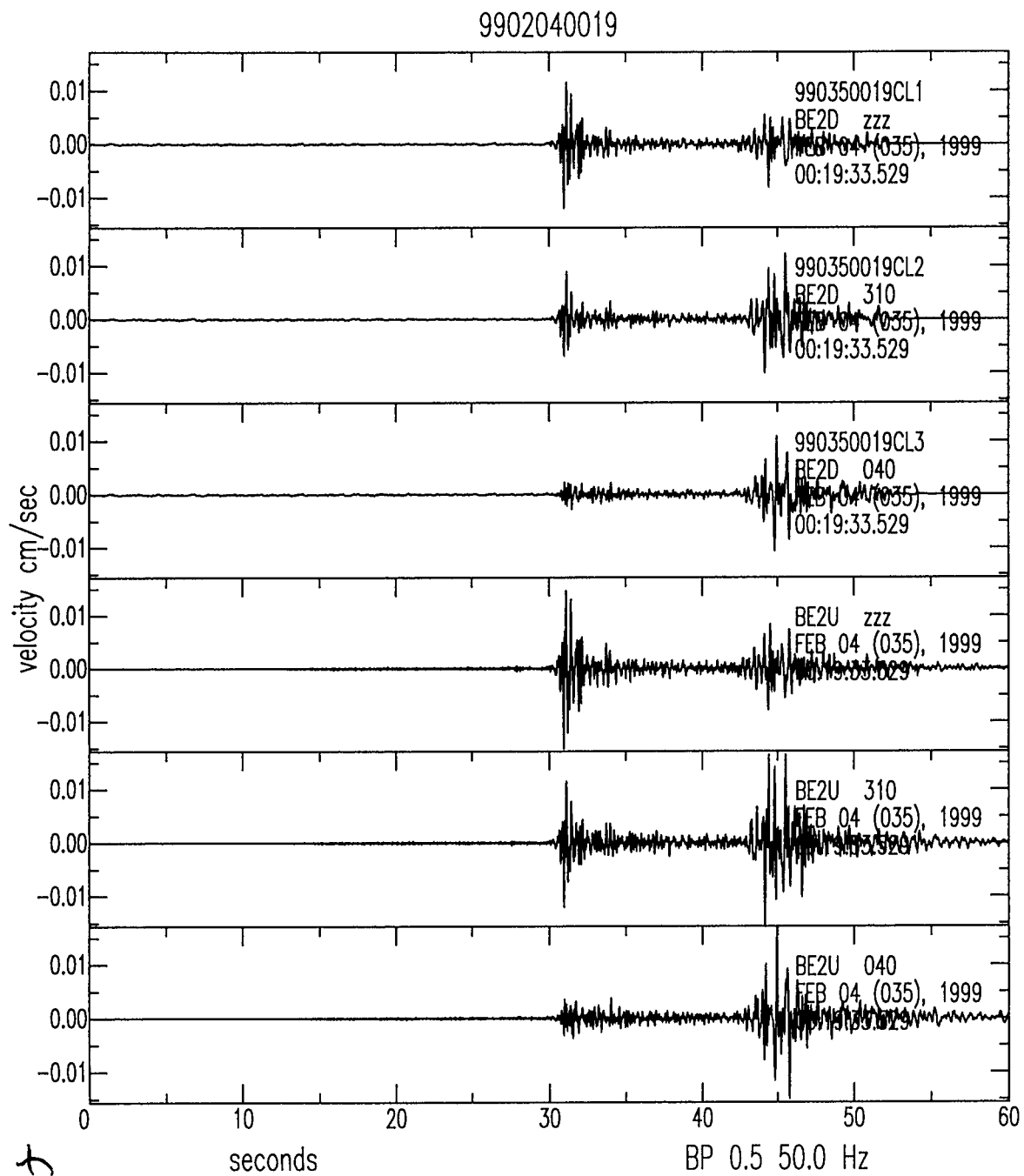


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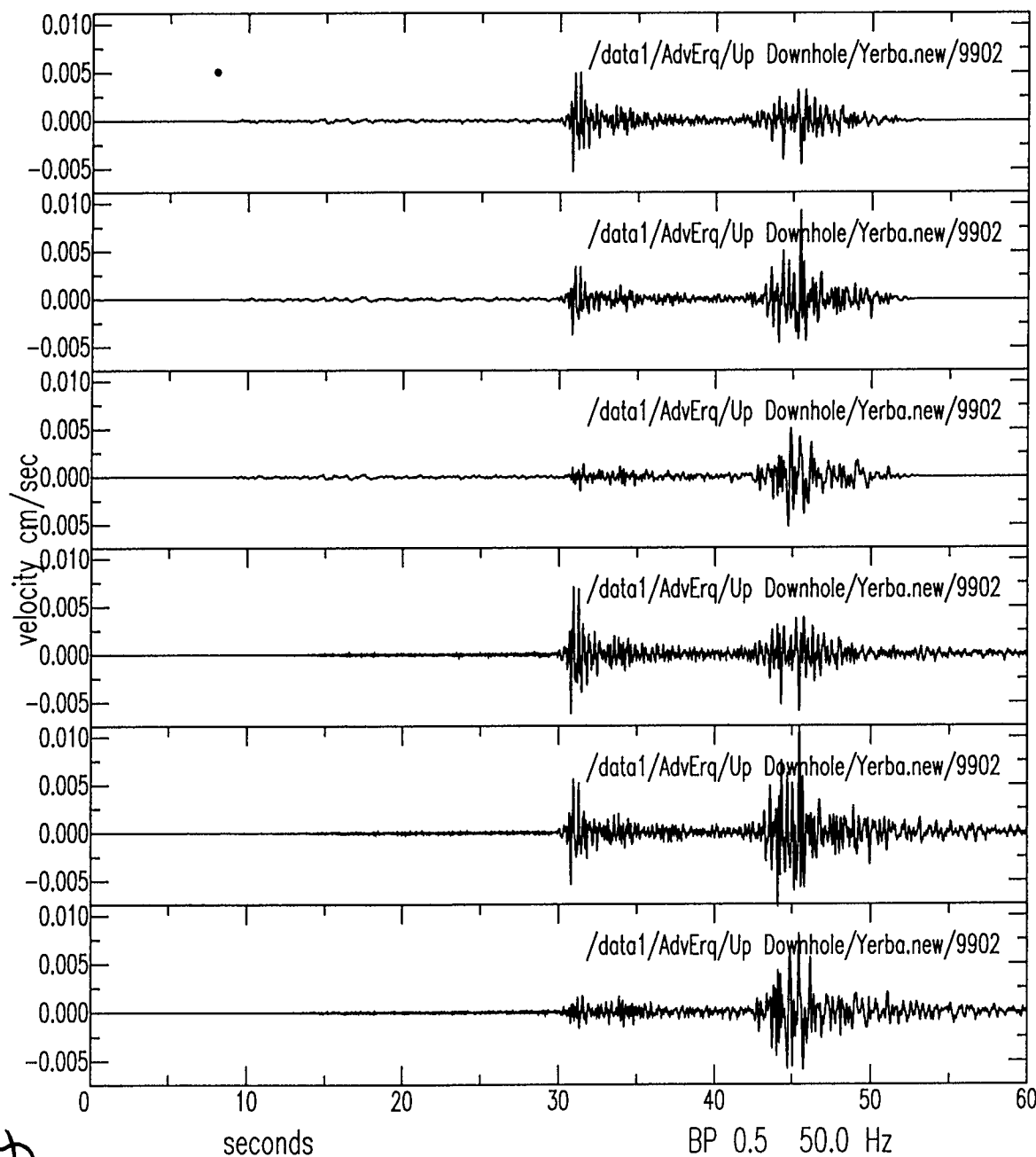
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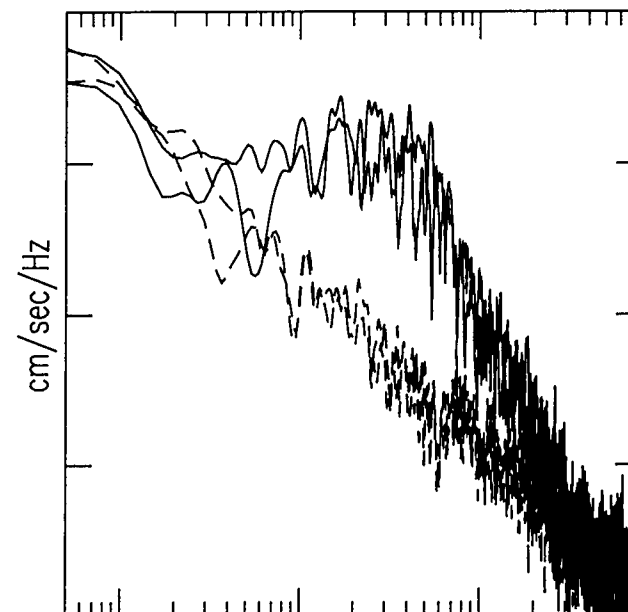


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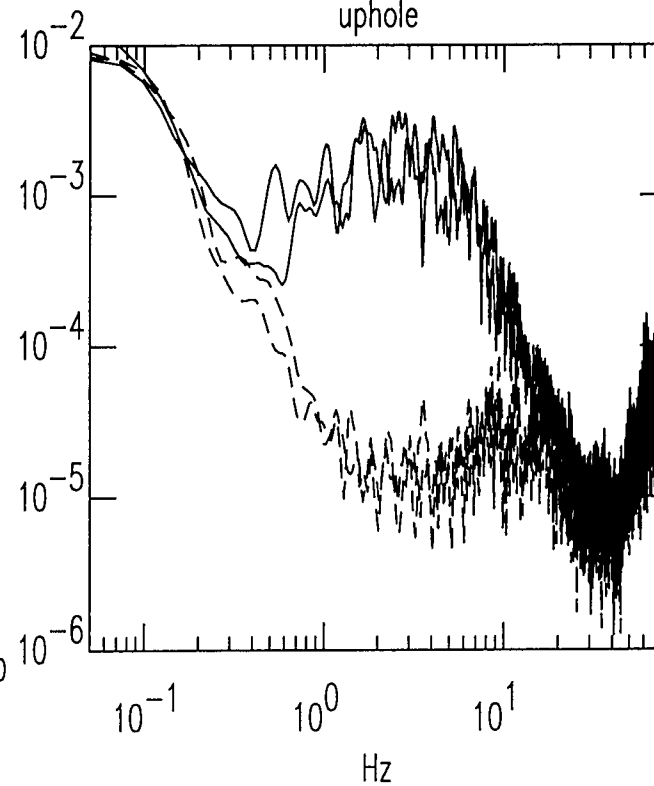
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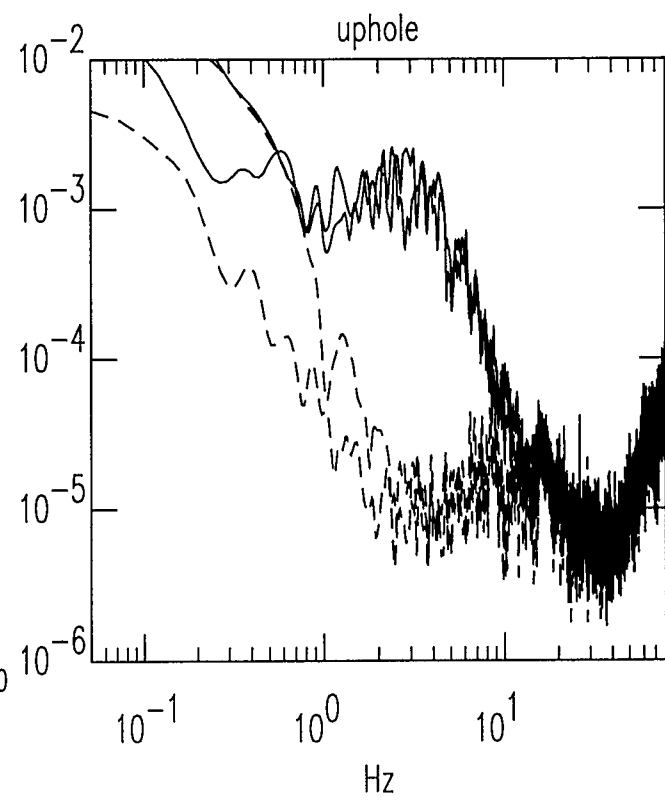
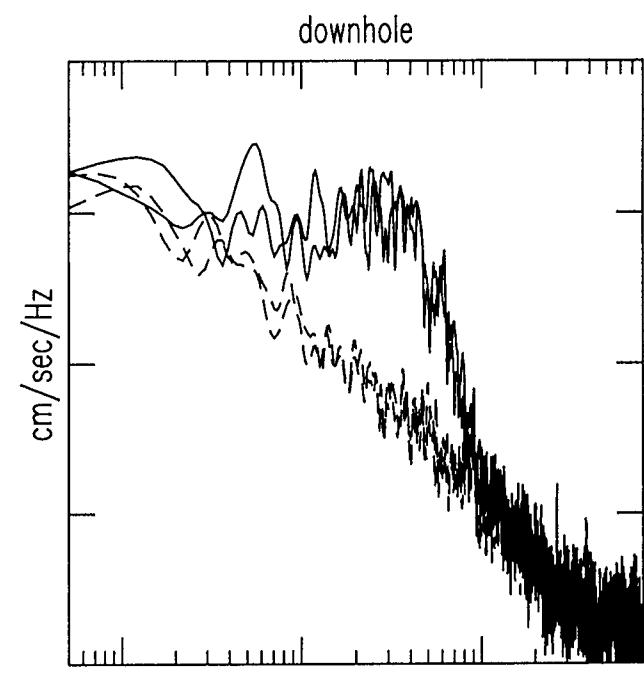
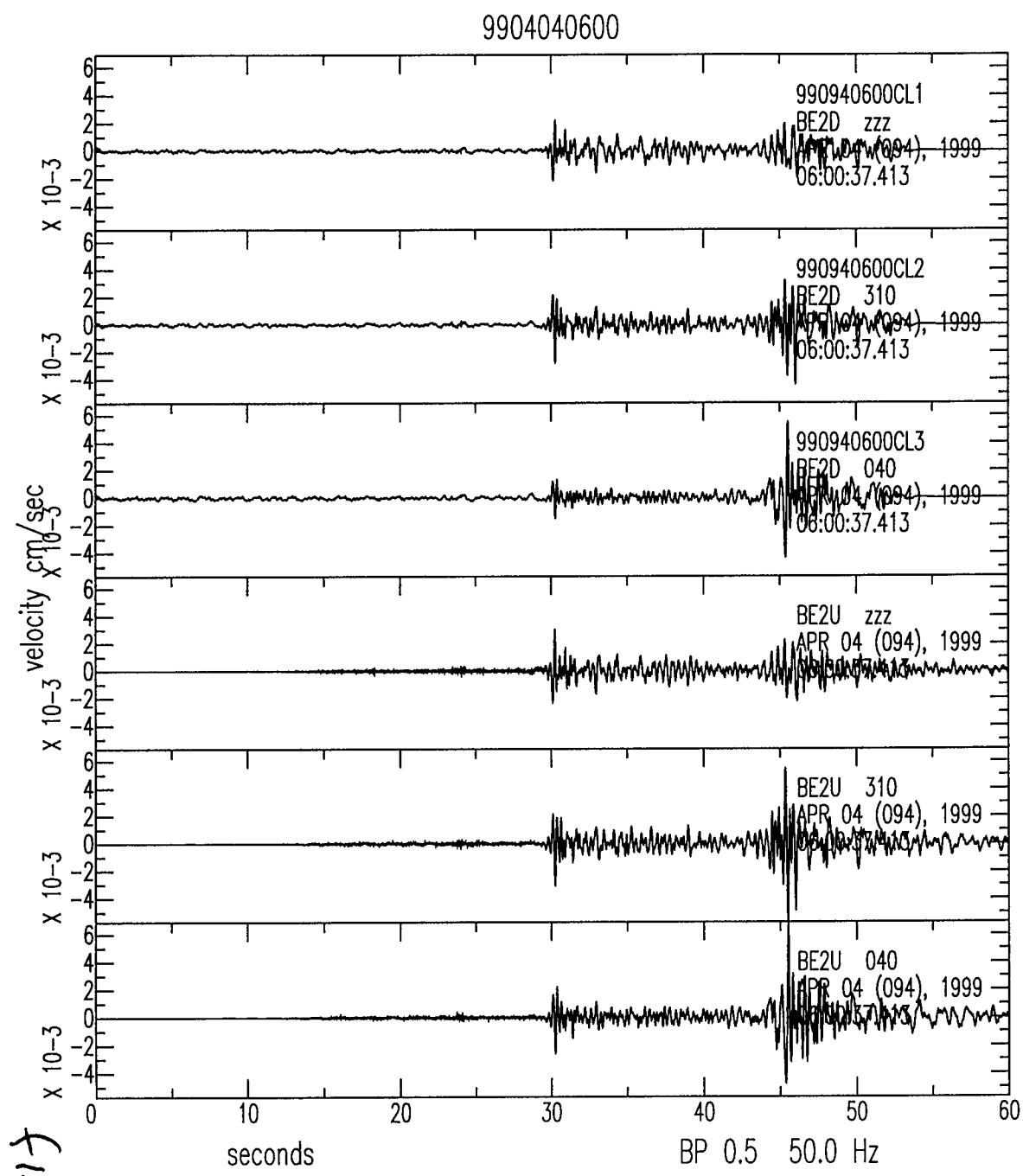


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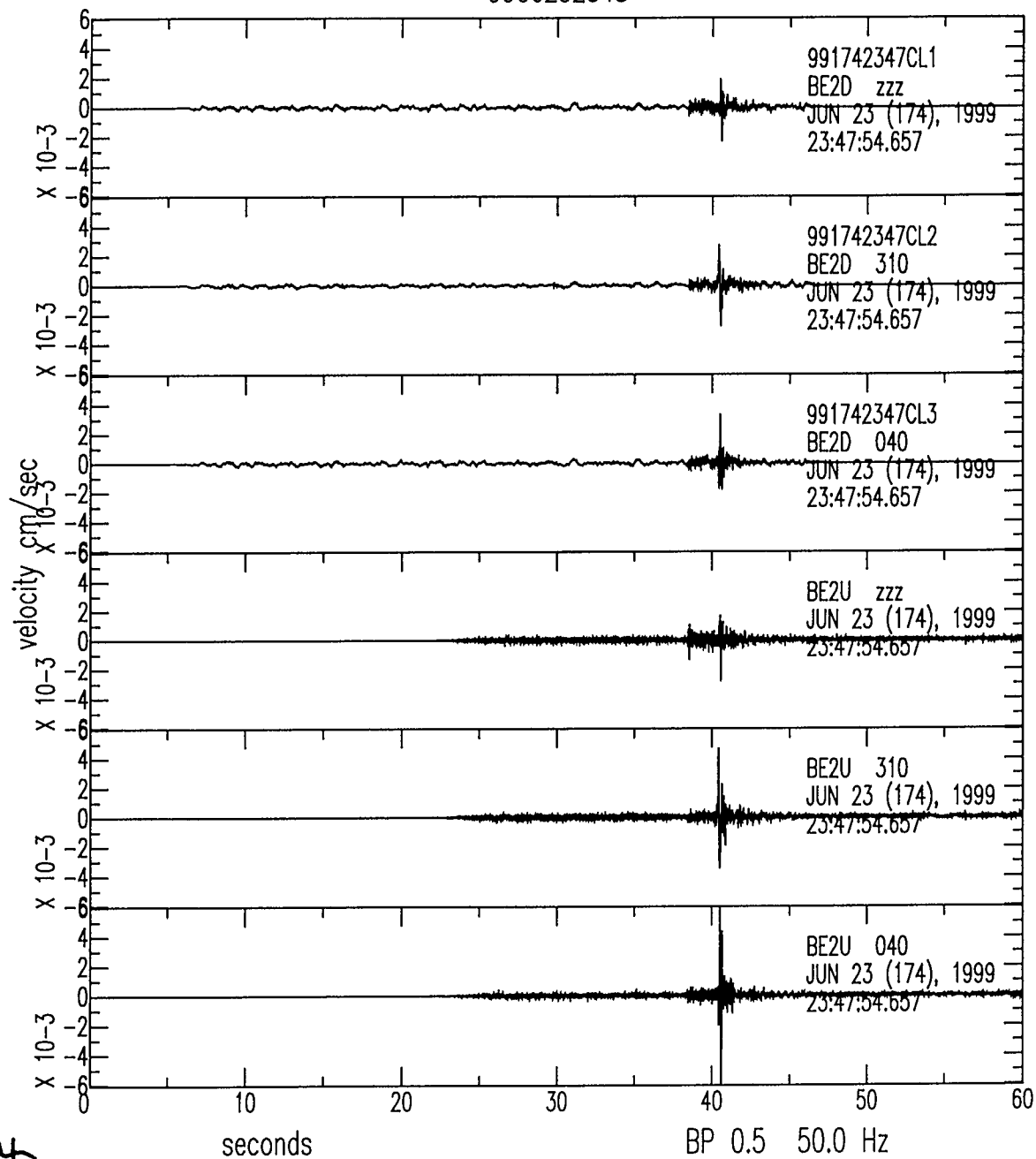


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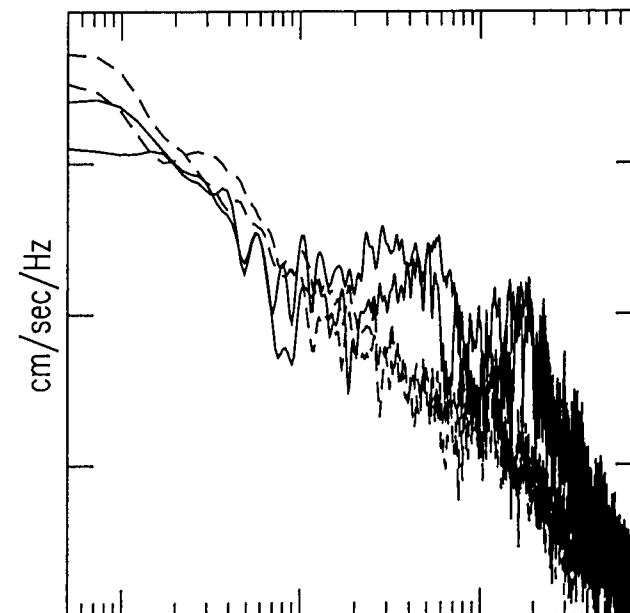
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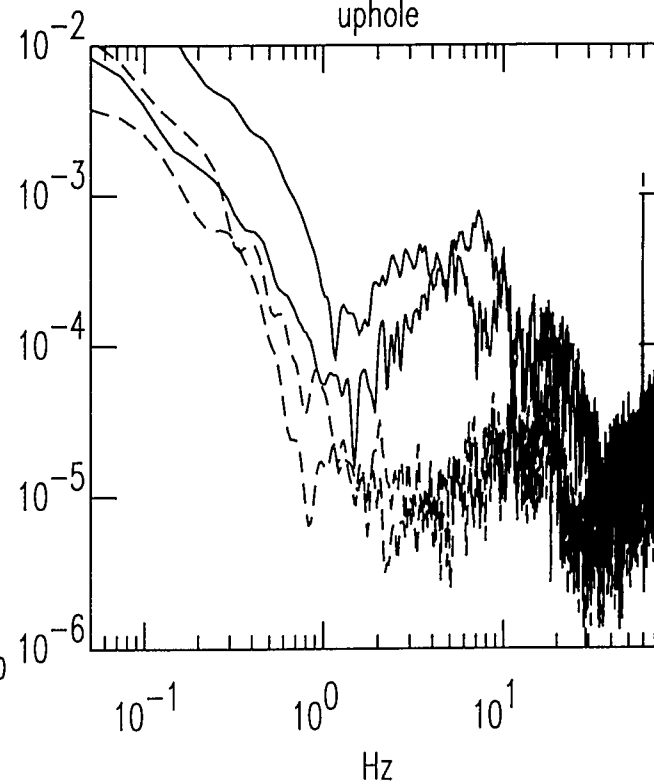
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downhole



uphole



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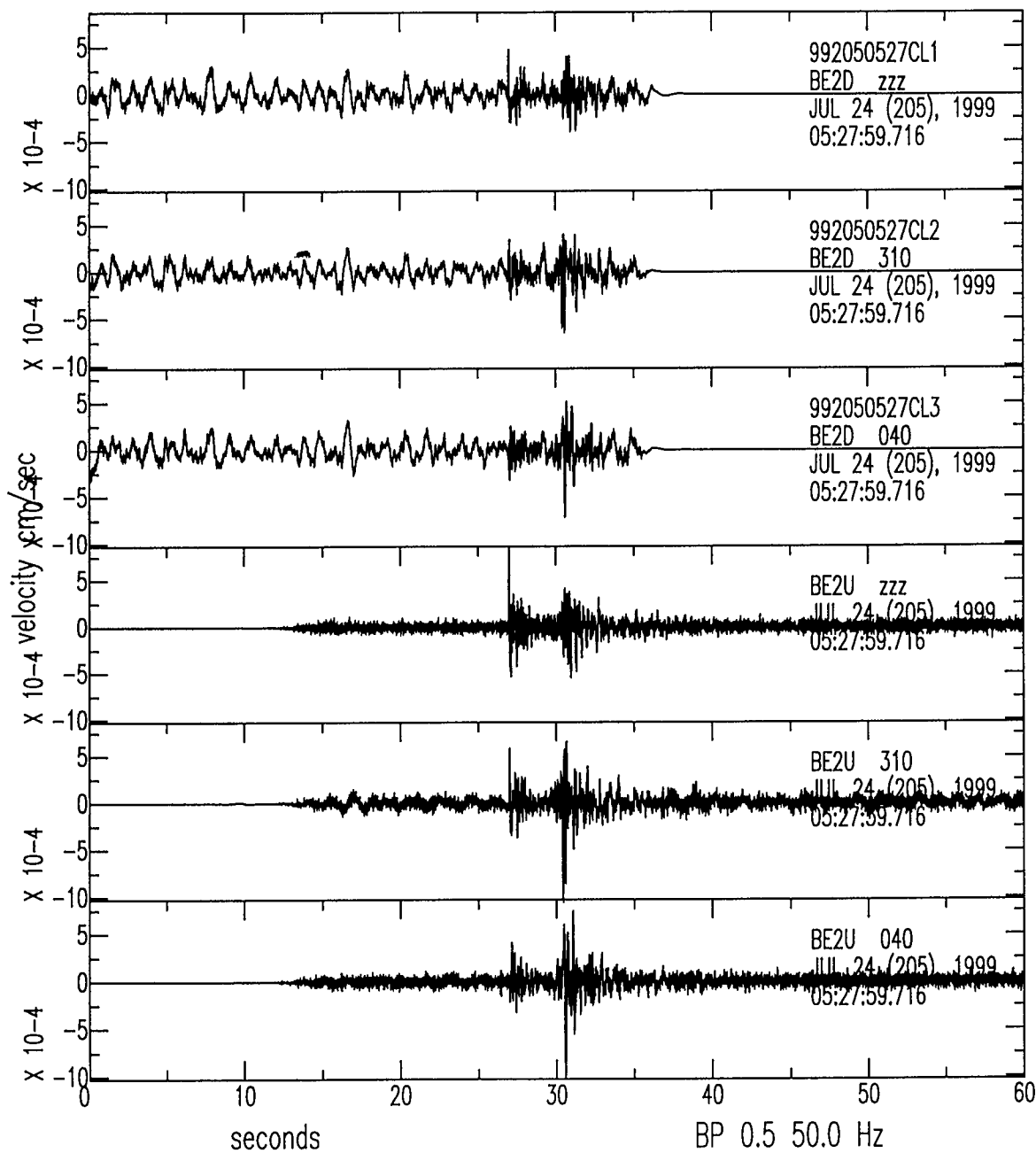
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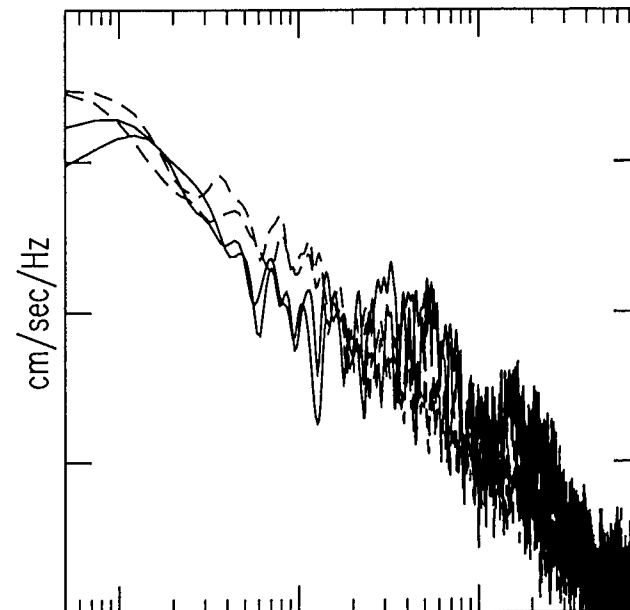
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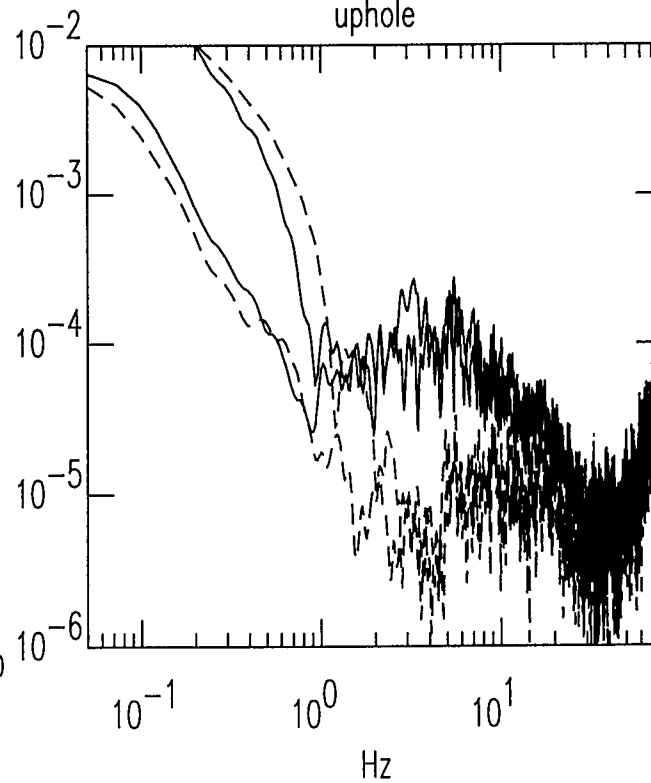
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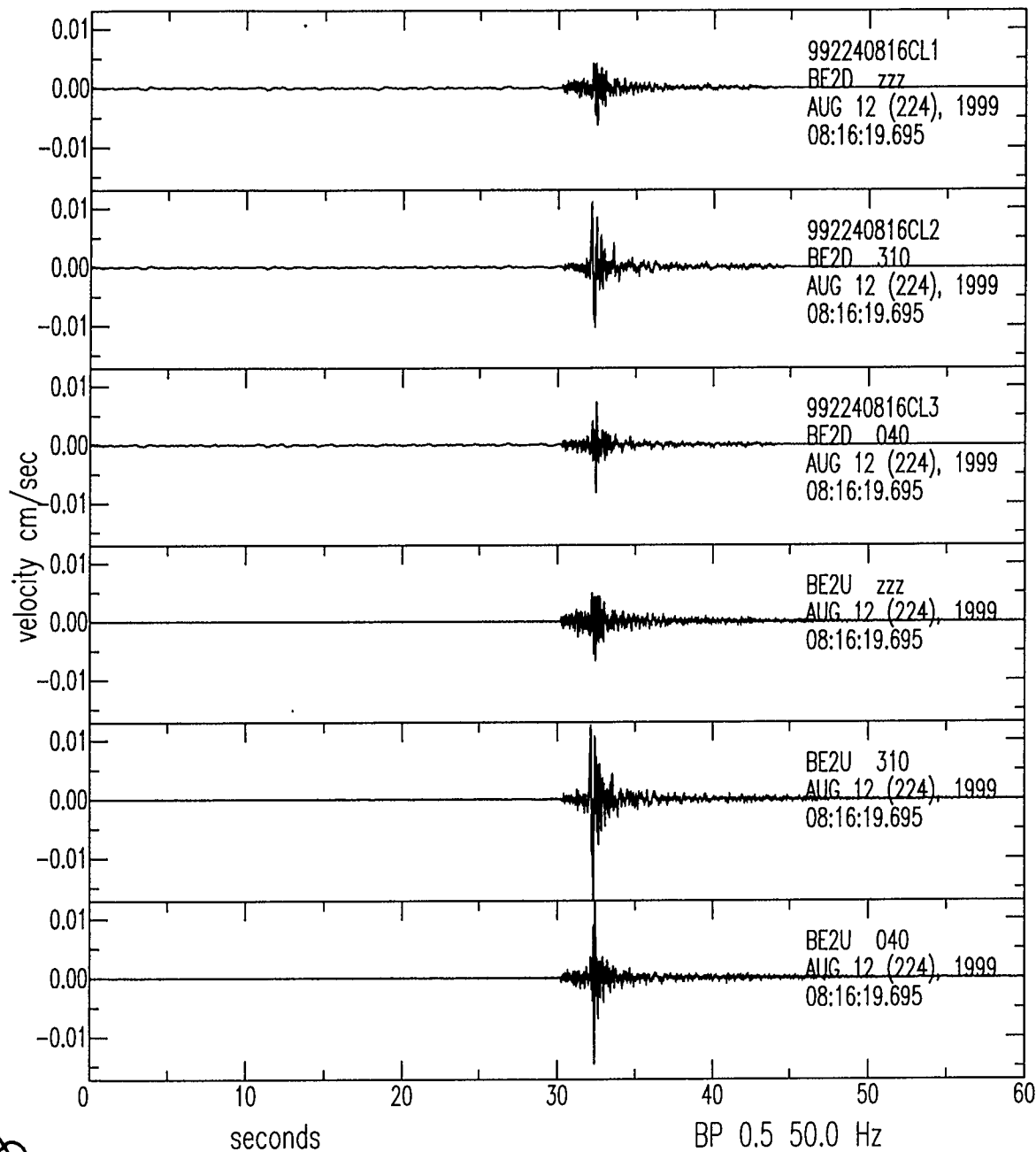


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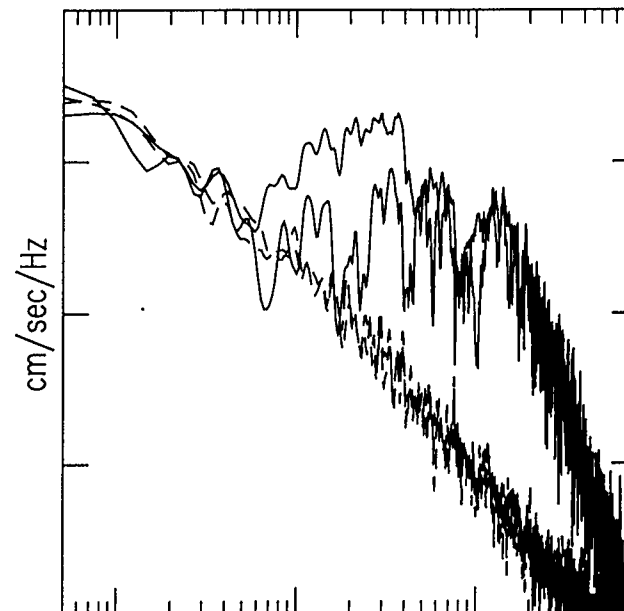


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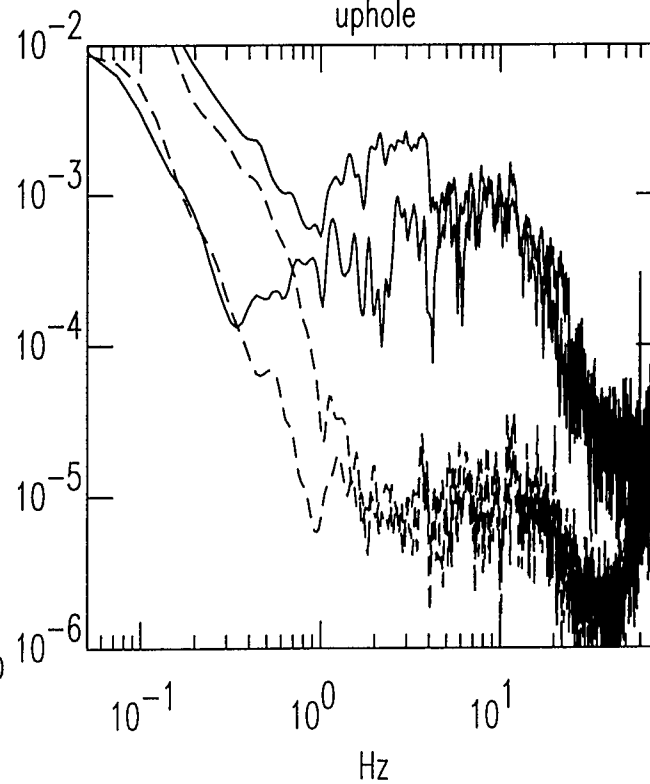
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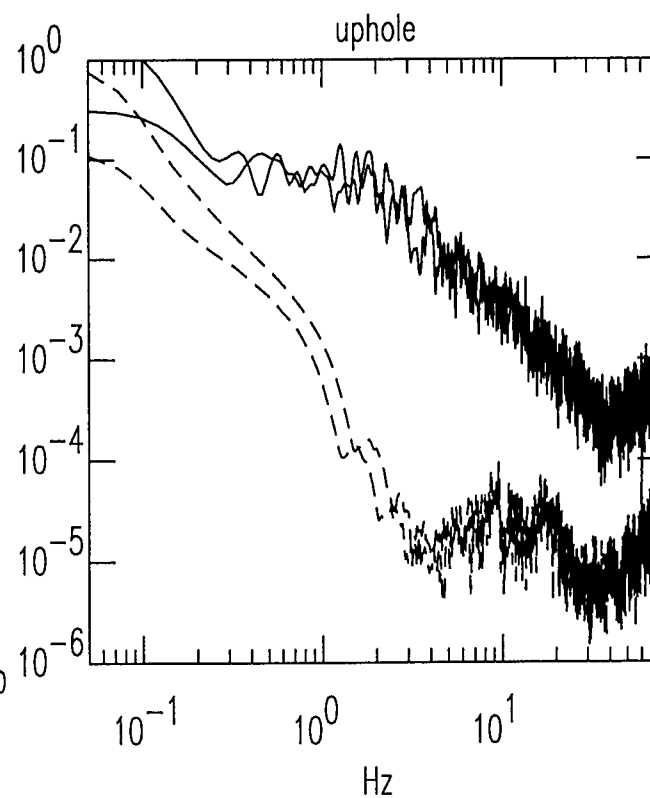
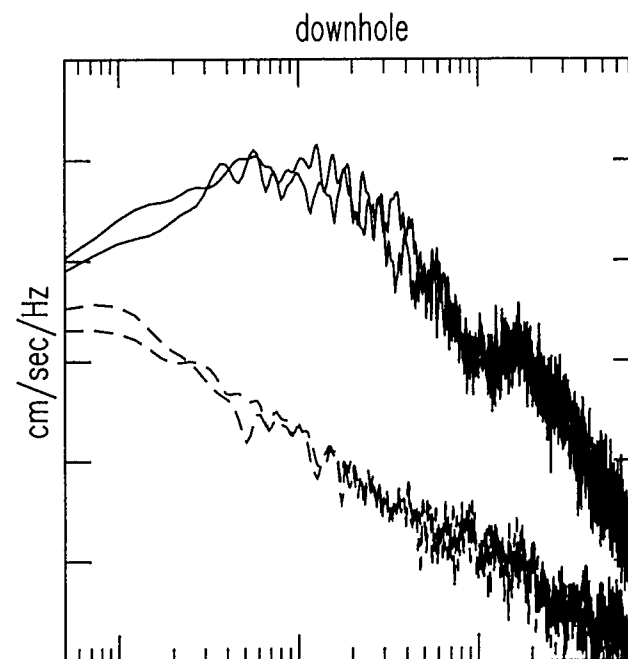
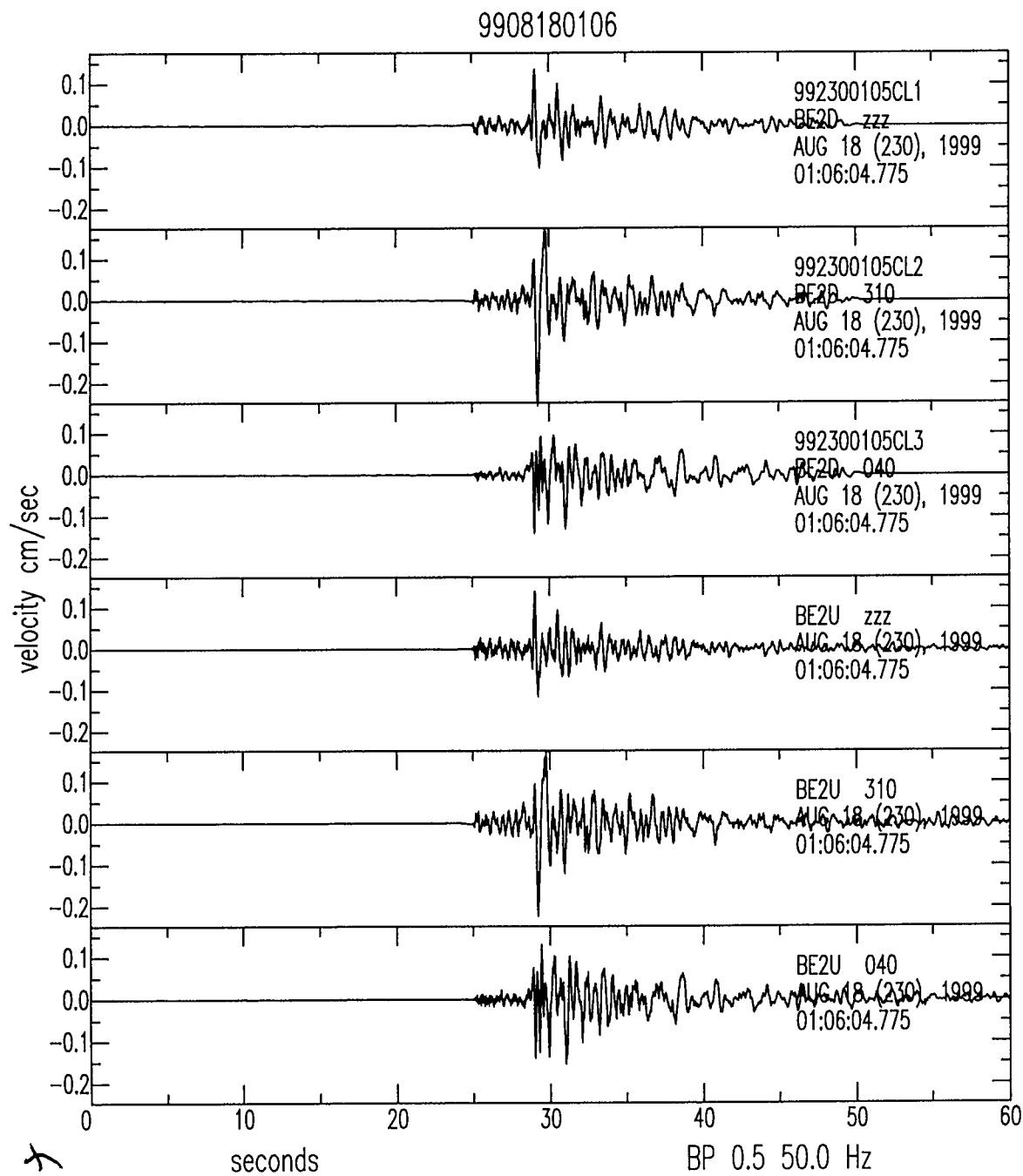


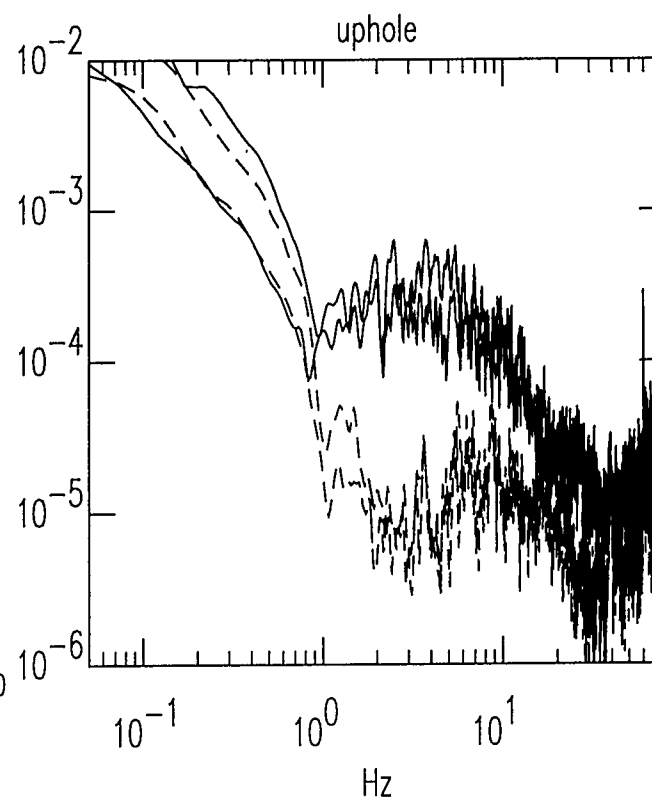
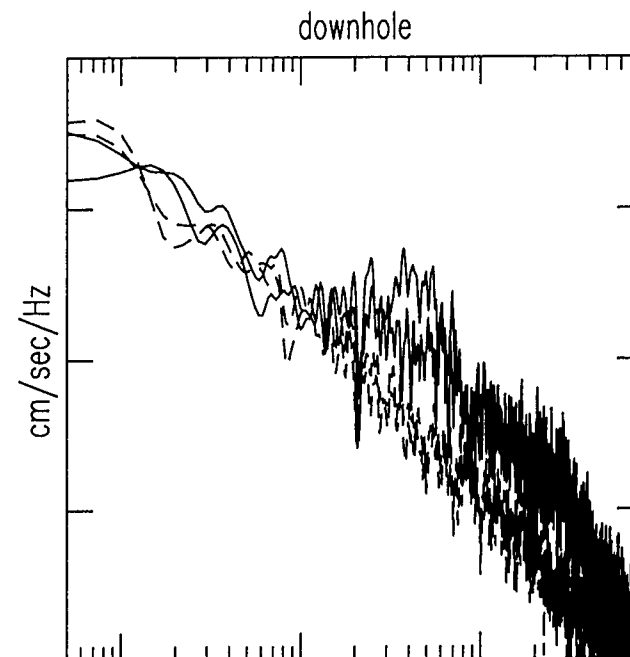
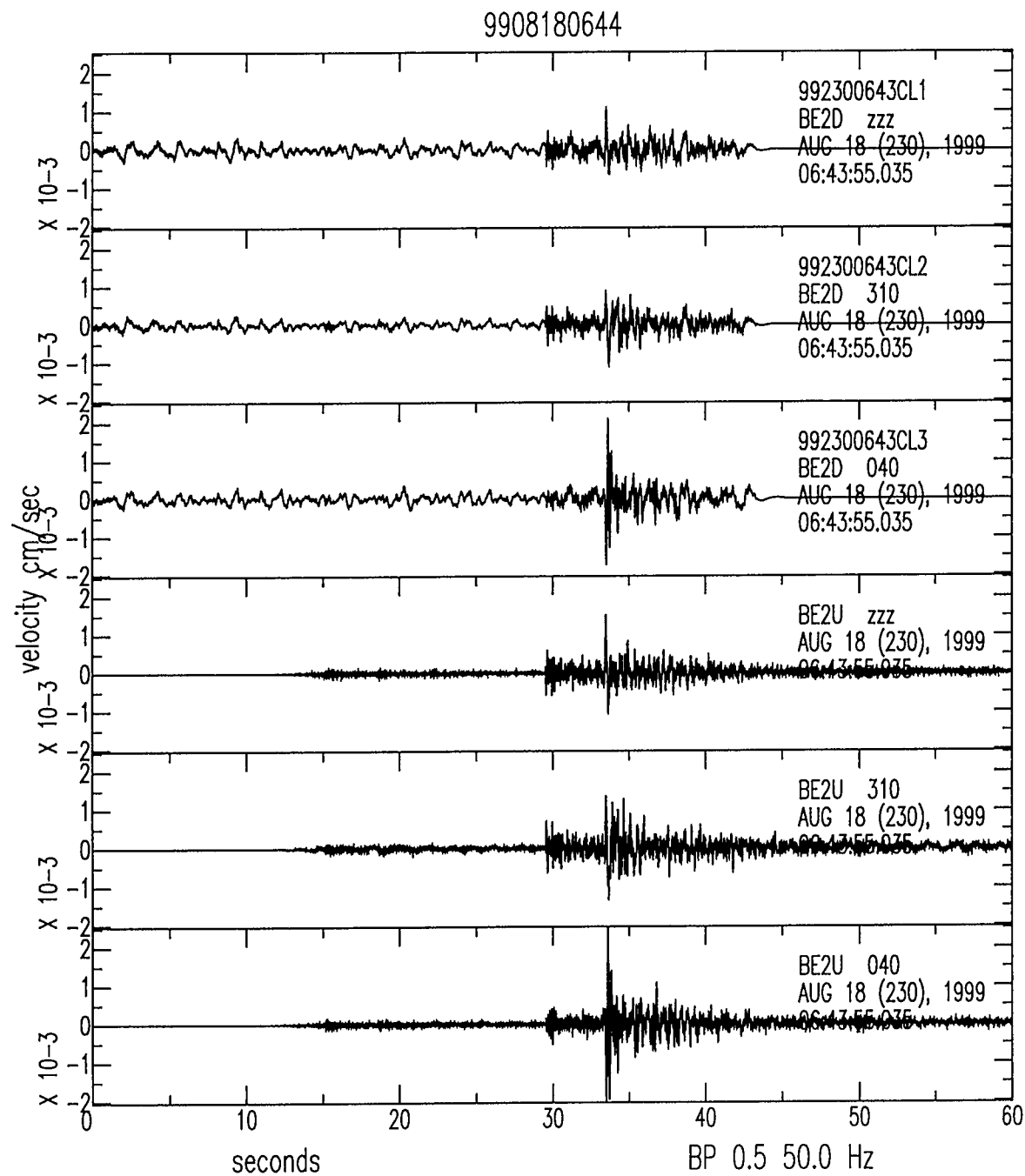
downhole



uphole







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